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PRELIMINARY
INSTRUCTION MANUAL

MODEL 427

CURRENT AMPLIFIER

KEITHLEY INSTRUMENTS

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We warrant each of our products to be free from defects in material and workmanship. Our obligation under this warranty is to repair or replace any instrument or part thereof which, within a year after shipment, proves defective upon examination. We will pay domestic surface freight costs.

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KEITHLEY INSTRUMENTS, INC.

INSTRUCTION MANUAL

MODEL 427

CURRENT AMPLIFIER

This Instruction Manual is supplied to permit earliest possible delivery of your instrument.

The Manual contains complete operating information. Also included are specifications, circuit description, replaceable parts list and schematics. The final edition will contain servicing and calibration information to maintain the instrument.

The Warranty Card attached to your instrument should be filled out and mailed so that the final edition can be sent to your personal attention. If you have further questions, please contact your Keithley Representative or the Sales Service Department, Cleveland, Ohio.

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SPECIFICATIONS

RANGE: 10^4 to 10^{11} volts per ampere in eight decade ranges. (10^{-13} ampere resolution to 10^{-3} ampere full output.)

OUTPUT: ±10 volts at up to 3 milliamperes. Output polarity is opposite input polarity.

OUTPUT RESISTANCE: Less than 10 ohms d-c to 30kHz.

OUTPUT ACCURACY: ±2% of reading to the 10^9 volts per ampere range, ±4% of reading on the 10^{10} and 10^{11} volts per ampere ranges exclusive of noise, drift and current offset.

RISE TIME (10% to 90%): Adjustable in 1x and 3.3x steps from "Fast Rise Time" listed below to 330 msec.

STABILITY: Current offset doubles per 10°C above 25°C. Voltage drift is less than 0.005% per °C and less than 0.005% per day of full output after 1-hour warm-up.

OFFSET CURRENT: Less than 10^{-12} ampere at 25°C and up to 70% relative humidity.

CURRENT SUPPRESSION: 10^{-10} ampere to 10^{-3} ampere in eight decade ranges with 0.1% resolution (10-turn potentiometer). Stability is ±0.2% of suppressed value per °C ±0.2% per day.

NOISE VS. RISE TIME*:

* With up to 100 pF input shunt capacitance. Noise and/or rise time increase as input shunt capacitance increases (1000 picofarads maximum).

INPUT VOLTAGE DROP: Less than 400μv for full-scale output on the 10^6 to 10^{11} volts per ampere ranges when properly zeroed.

EFFECTIVE INPUT RESISTANCE: Less than 15 ohms on the 10^4 and 10^5 volts per ampere ranges, increasing to less than 4 megohms on the 10^{11} volts per ampere range.

MAXIMUM INPUT OVERLOAD:

Transient: 1000 volts on any range for up to 3 seconds using a Keithley (or other 10mA -limited) high-voltage supply.

Continuous: 500 volts on the 10^{11} to 10^7 volts per ampere ranges, decreasing to 200 volts on the 10^6, 70 volts on the 10^5, and 20 volts on the 10^4 volts per ampere ranges.

OVERLOAD INDICATION: Lamp indicates pre-filter or post-filter overload.

DYNAMIC RESERVE: 10 (20dB)

CONNECTORS:

Input: BNC (Front)
Output: BNC (Front and rear)

POWER: 90-125 volts (or 180-250 v, switch selected), 50-60 Hz, 5 watts.

DIMENSIONS; WEIGHT: Overall bench size - 4" high x 8-1/2" wide x 12-1/8" deep (100 x 217 x 310mm); (Style "M" 3-1/2" half-rack). Net weight, 7 lbs. (3,0 kg).

	FAST RISE TIME			WIDE DYNAMIC RANGE		
GAIN V/A	RISE TIME (10%-90%)	DYNAMIC RANGE	NOISE (ampere rms)	DYNAMIC RANGE	NOISE (ampere rms)	RISE TIME (10%-90%)
10^{11}	1500 μs	100	$4x10^{-13}$	13000	$3x10^{-15}$	330 ms
10^{10}	400 μs	200	$2x10^{-12}$	20000	$2x10^{-14}$	100 ms
10^9	220 μs	400	$1x10^{-11}$	20000	$2x10^{-13}$	10 ms
10^8	60 μs	800	$5x10^{-11}$	20000	$2x10^{-12}$	1 ms
10^7	40 μs	2000	$2x10^{-10}$	20000	$2x10^{-11}$	100 μs
10^6-10^4	15 μs	2000	----	20000	----	100 μs

SECTION 1. GENERAL DESCRIPTION

1-1. GENERAL. The Model 427 Current Amplifier is a high-speed, feedback-type amplifier with particular features useful for automated semiconductor testing, mass spectrometry, and gas chromatography applications.

1-2. FEATURES.

a. Wide Dynamic Range. Selectable rise times permit low-noise operation important when resolving small current levels.

b. High Speed. Typical resolution is 20 picoamperes out of a 10^{-8} ampere signal with a 100 microsecond rise time.

c. Built-in Current Suppression. Small changes in the signal level can be measured since large ambient current levels can be easily suppressed.

d. Overload Indication. Accurate measurements are assured since overloads are automatically indicated.

e. Variable Gain. The GAIN Switch is designated in eight gain positions from 10^4 to 10^{11} volts per ampere - therefore gain adjustment is straight forward.

f. Variable Rise Time. Optimum response can be selected for each gain setting since a separate RISE TIME switch is provided on the front panel.

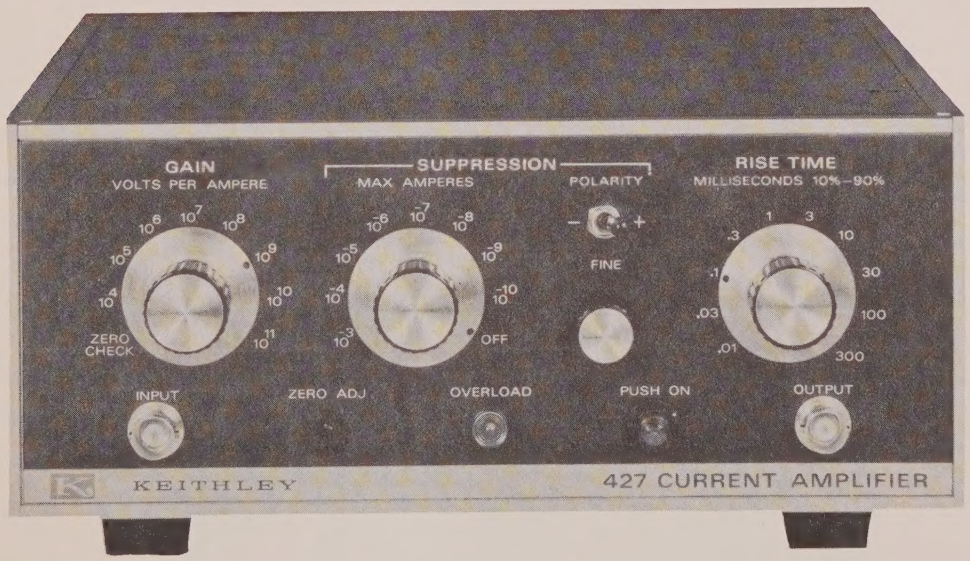


TABLE 1-1.
Front Panel Controls and Terminals

Control or Terminal	Functional Description	Paragraph
PUSH ON Power Switch (S302)	Controls power to instrument.	2-4, a1
GAIN Switch (S201)	Sets gain in volts per ampere.	2-4, a2
RISE TIME (S101)	Sets rise time in milliseconds.	2-4, a3
SUPPRESSION		
MAX AMPERES Switch (S303)	Sets maximum suppression.	2-4, a4
FINE Control (R333)	Adjusts suppression.	2-4, a5
POLARITY Switch (S304)	Sets polarity of suppression.	2-4, a6
ZERO ADJ Control (R235)	Adjusts output zero.	2-4, a7
INPUT Receptacle (J202)	Input source connection.	2-3, a
OUTPUT Receptacle (J102)	Output connection.	2-3, b
OVERLOAD Indicator (DS302)	Indicates overload condition.	2-5, d

TABLE 1-2.
Rear Panel Controls and Terminals

Control or Terminal	Functional Description	Paragraph
Line Switch (S301)	Sets instrument for 117V or 234V.	2-4, b
Power Receptacle (P305)	Connection to line power.	2-3, c
Fuse (F301)	Type 3AG Slow-Blow, 117V @ 1/4 A 234V @ 1/8 A	- -
OUTPUT Receptacle (J103)	Output Connection.	2-3, b

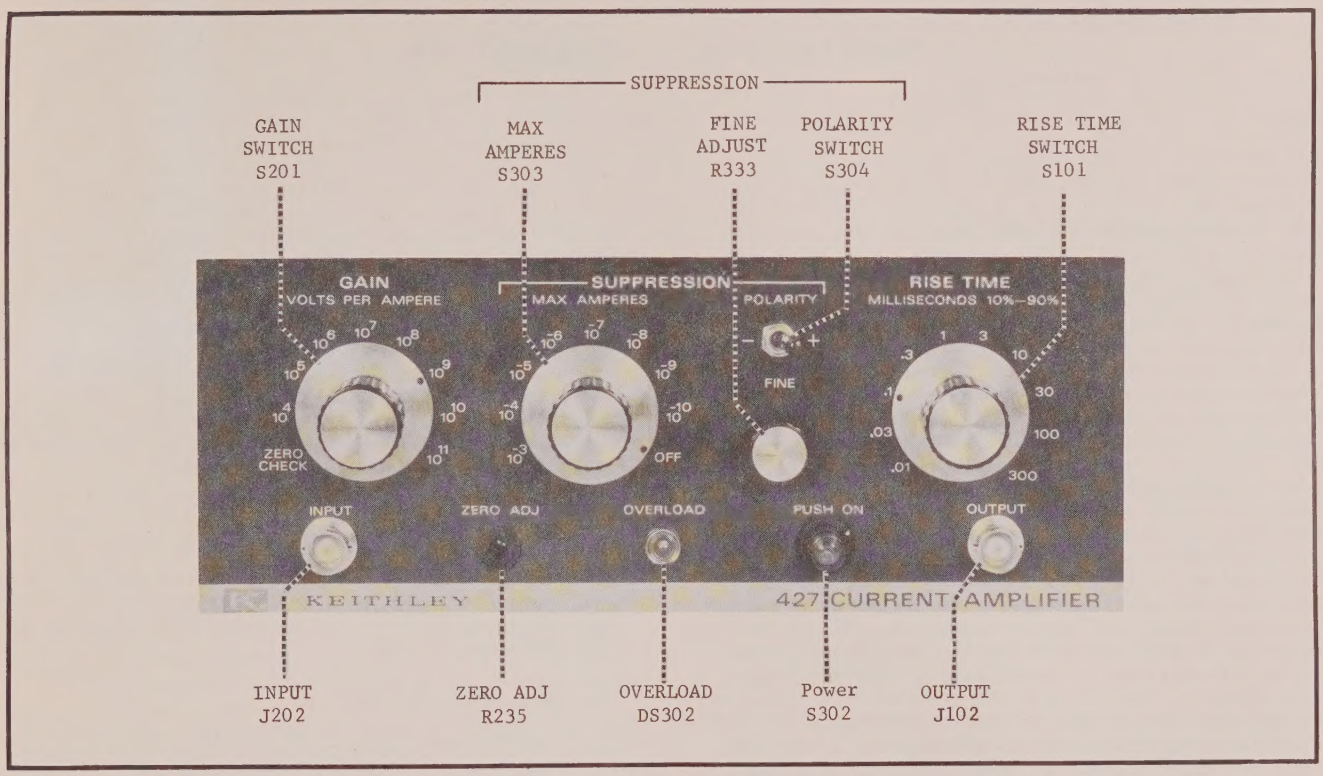


FIGURE 2. Front Panel Controls.

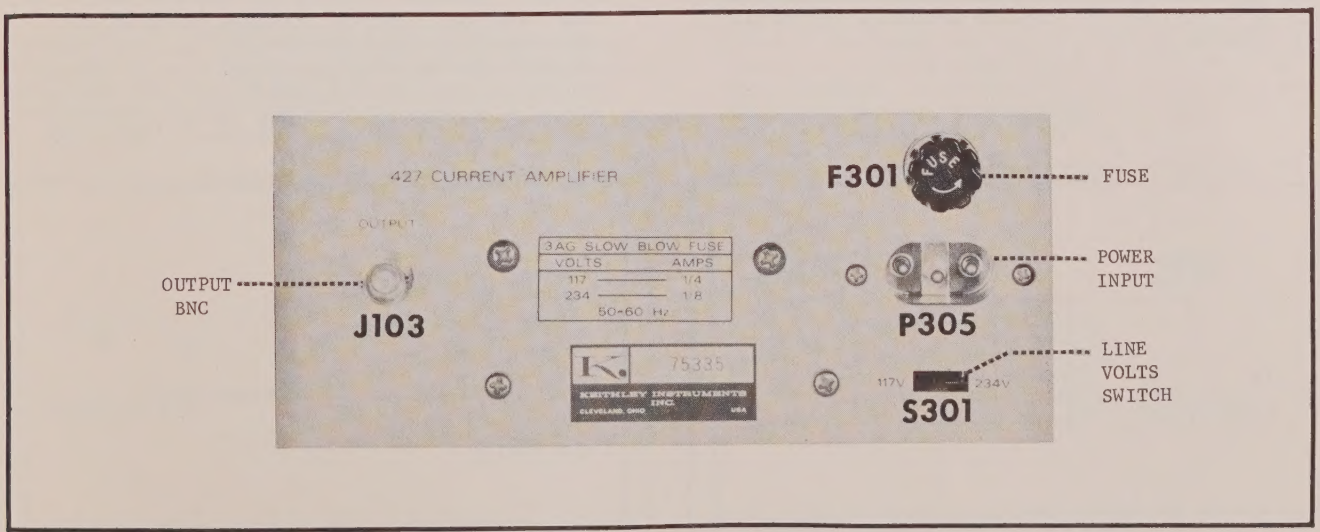


FIGURE 3. Rear Panel Controls.

SECTION 2. OPERATION

2-1. MEASUREMENT CONSIDERATIONS.

a. Current-Detection Devices. The measurement of small electrical currents has been the basis for a number of instrumental methods used by the analyst. Ion chambers, high-impedance electrodes, many forms of chromatographic detectors, phototubes and multipliers are commonly-used transducers which require the measurement of small currents. Devices used for this measurement are often called electrometers.

b. Current-Detection Limitations. In any measurement, if source noise greatly exceeds that added by the instrumentation, optimization of instrumentation is unimportant. When source noise approaches theoretical minimum, optimization of instrumentation characteristics becomes imperative. To determine the category into which this measurement falls, the researcher needs to be familiar with the characteristics which impose theoretical and practical limitations on his measurement. Most researchers are familiar with the theoretical limitations present in voltage measurements. The noise increases with source resistance, and the familiar equation for the mean-square noise voltage is

$$\overline{e_n}^2 = 4kTR\,\Delta f \qquad \text{Eq. 1}$$

where k is the Boltzmann Constant, T is the absolute temperature of the source resistance R, and Δf is the noise bandwidth ($\frac{\pi}{2}$ times the 3 dB bandwidth for a single RC rolloff.) In the case of current measurements it is more appropriate to consider the noise current generated by the source and load resistances. The mean square noise current generated by a resistor is given by Eq. 2.

$$\overline{i_n}^2 = \frac{4kT\,\Delta f}{R} \qquad \text{Eq. 2}$$

From this equation it is immediately apparent that the measurement of small current requires large values of R, i.e., high impedance levels. However, this gives difficulties for measurements requiring wide bandwidths because of the RC time constant associated with a high-megohm resistor and even a few picofarads of circuit capacitance. Figure 4 shows a current source generating a voltage across a parallel RC. The frequency response of this current measurement is limited by the RC time constant. Figure 5 shows this response and the -3 dB point occurs at a frequency

$$F_o = \frac{1}{2\pi RC} \qquad \text{Eq. 3}$$

Low noise and high speed, therefore, are contradictory requirements. To optimize a current-measuring system, techniques must be used which obtain high speed using high-impedance devices.

c. High Speed Methods.

1. High speed can, of course, be obtained in a shunt-type measurement by using a low value for the shunt resistor. As pointed out above, such a small resistor value introduces excessive noise into the measurement.

2. A second method to achieve bandwidth is to keep R large, to accept the frequency roll-off starting at F_o, and to change the frequency response of the voltage amplifier as shown in Figure 6a. The combined effects of the RC time constant followed by this amplifier is shown in Figure 6b and it is seen that the frequency response of the current measurement has been extended to F_1. The frequency at which the amplifier gain starts to increase must be exactly equal to the frequency F_o determined by the RC time constant in order for this approach to result in a flat frequency response. Therefore,

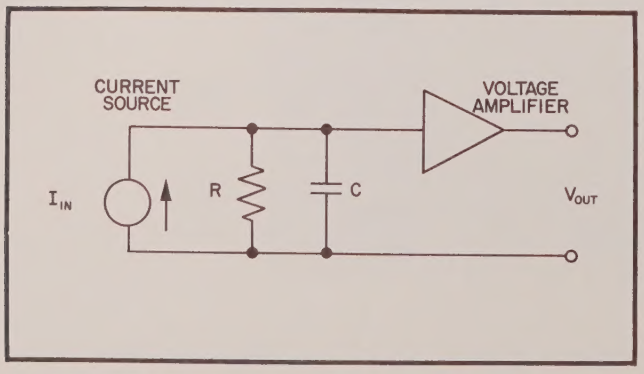


FIGURE 4. In the shunt method current is measured by the voltage drop across a resistor.

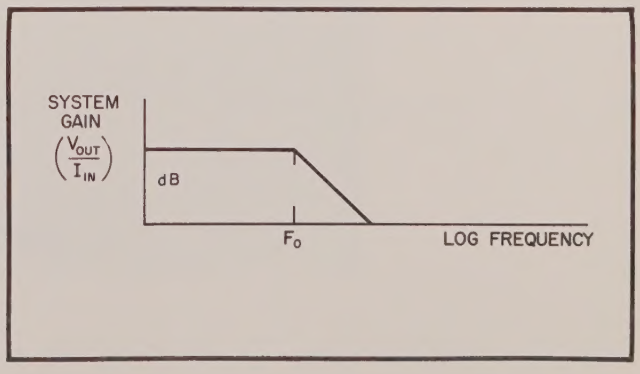


FIGURE 5. The frequency response of the shunt method is limited by omnipresent shunt capacitance.

this method is useful only for applications where the shunt capacitance C is constant. Aside from this drawback this is a legitimate approach which is being used in low-noise, high-speed current-measuring applications. In addition to current noise in the shunt and in the amplifier input stage, a major source of noise in this system arises from the voltage-noise generator associated with the input stage (reflected as current noise in the shunt resistor) caused by the high-frequency peaking in the following stages of amplification. More will be said about this in the discussion on noise behavior.

3. A third method used for speeding up a current measurement uses guarding techniques to eliminate the effects of capacitances. Unfortunately only certain types of capacitances, such as cable capacitances, can be conveniently eliminated in this manner. To eliminate the effect of parasitic capacitances associated with the source itself becomes very cumbersome and may not be feasible in many instances. The major sources of noise in this system are identical to those mentioned in the second system.

4. A fourth circuit configuration combines the capability of low-noise and high-speed performance with tolerance for varying input C and eliminates need for separate guard by making the ground plane an effective guard. This is the current-feedback technique. This technique gives a typical improvement of 3 over shunt techniques. Again, the major sources of noise are identical to those mentioned in the second system.

d. Noise in Current Measurements. Noise forms a basic limitation in any high-speed current-measuring system. The shunt system gives the simplest current measurement but does not give low-noise performance. A properly designed feedback system gives superior noise - bandwidth performance. Noise in these two systems will be discussed next.

1. Noise Behavior of the Shunt System. High speed and low noise are contradictory requirements in any current measurement because some capacitance is always present. The theoretical performance limitation of the shunt system can be calculated as follows:

The rms thermal noise current (i_n) generated by a resistance R is given by

$$i_n = \sqrt{\frac{4kT}{R} \Delta f} \qquad \text{Eq. 4}$$

The equivalent noise bandwidth (Δf) of a parallel RC combination is $\Delta f = 1/(4RC)$ and the signal bandwidth (3 dB bandwidth) $F_o = 1/(2\pi RC)$. For practical purposes peak-to-peak noise is taken as 5 times the rms value. The peak-to-peak noise current can now be written as

$$i_{npp} = 2 \times 10^{-9} F_o \sqrt{C} \qquad \text{Eq. 5}$$

In practice, a typical value for shunt capacitance is 100 picofarads. With this value the following rule-of-thumb is obtained. The lowest ratio of detectable current divided by signal bandwidth using shunt techniques is $2 \cdot 10^{-14}$ ampere/Hertz for a peak-to-peak signal-to-noise ratio equal to 1. A corollary for this rule-of-thumb expresses the noise current in terms of obtainable risetime (10-90% risetime $t_r = 2.2$ RC). The lowest product of detectable current and risetime using shunt techniques is 7×10^{-15} ampere seconds. In this derivation it has been assumed that the voltage amplifier does not contribute noise to the measurement.

2. Noise Behavior of the Feedback System. There are three sources of noise in the feedback system that have to be looked at closely. The first two, input-stage shot noise and current noise from the measuring resistor, are rather straight-forward. The third, voltage noise from the input device of the amplifier, causes some peculiar difficulties in the measurement. Any resistor connected to the input injects white current noise (Eq. 4). In the circuit of Figure 7 the only resistor that is connected to the input is the feedback resistor R. As in the shunt system, R must be made large for lowest noise. Because this noise is white, the total contribution can be calculated by equating Δf to the equivalent noise bandwidth of the system. The second source of noise is the current noise from the amplifier input. This component is essentially the shot noise associated with the gate leakage current (i_o) of the input device. Its rms value equals ...

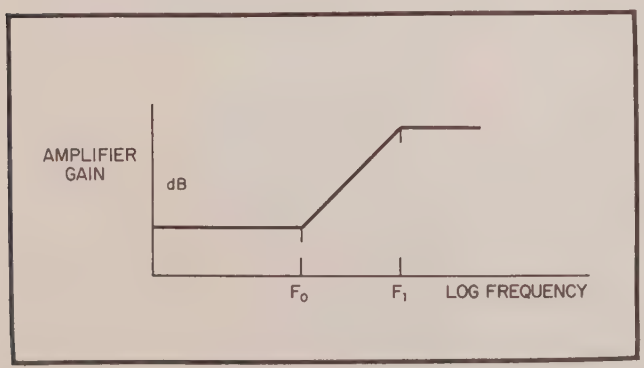


FIGURE 6. By tailoring the frequency response of the amplifier (Fig. 6a) the frequency response of the shunt method can be extended.

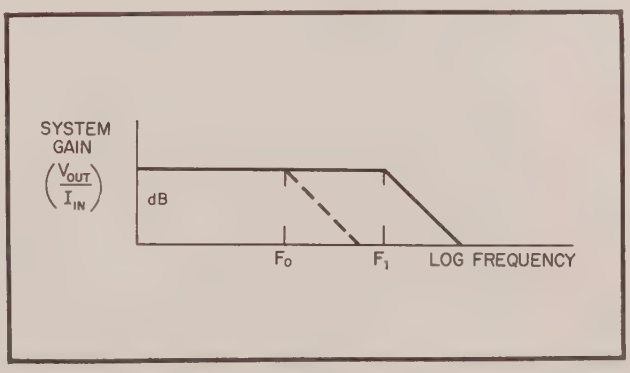


FIGURE 6b. Extended frequency response.

$$\overline{i_n} = \sqrt{2\, e\, i_o\, \Delta f} \qquad \text{Eq. 9}$$

where e is the electronic charge. The contribution of this noise generator is also white. Not only do these two noise sources generate white current noise, the noise in a given bandwidth is also independent of the input capacitance C. The major source of noise in a feedback current measurement is the noise contribution associated with the voltage noise of the input amplifier. The voltage noise can be represented by a voltage noise generator (e_n) at the amplifier input as shown in Figure 8. This noise generator itself is assumed to be white. However, its total noise contribution to the current-measuring system is not white. Inspection of Figure 8 will reveal that at low frequencies a large amount of feedback is applied around the voltage noise source (e_n). However, the RC combination attenuates the high-frequency components of V_{out} so that no feedback is present at high frequencies. Thus, the noise contribution to the output voltage V_{out} from the voltage noise source e_n is no longer independent of frequency. The noise is "colored" and increases in intensity for all frequencies higher than F_o. The resulting noise spectrum is shown in Figure 9b. The total system noise is related to the area under this curve. Because the logarithm of frequency is plotted on the horizontal axis, the area under the curve at higher frequencies represents a significantly larger amount of noise than a similar area at low frequencies. For comparison, Figure 9a shows the frequency response of the current measuring system. Figure 9a is identical to Figure 6b. It is interesting at this point to compare this noise spectrum with the frequency response of the voltage amplifier in Figure 4 as shown in Figure 6a. A voltage noise source at the input of the amplifier would generate a noise spectrum according to the amplifier frequency response as shown in Figure 6a. The noise spectrum of such a system, then, is identical to the noise spectrum of the feedback system as given in Figure 9b. This illustrates the well-known fact that signal-to-noise performance of a measurement cannot be improved by feedback techniques. At the high-frequency end the voltage noise is limited by the frequency F_A which is the high-frequency roll-off point of the operational amplifier. It should be noted that even though the useful bandwidth of the system extends only to F_1, there are noise components of higher frequency present. To obtain best wideband-noise performance, these high-frequency noise components have to be removed. This can be achieved by adding a low-pass filter section following the feedback input stage. If the band-pass of this low-pass filter is made adjustable this filter can serve the dual purpose of removing high-frequency noise and of limiting the signal bandwidth of the system.

2-2. THEORY OF OPERATION.

a. Current Feedback Technique. The basic circuit configuration used in the current-feedback technique is shown in Figure 7. In this configuration the current-measuring resistor R is placed in the feedback loop of an inverting amplifier with a gain of A_o. The frequency response obtained with this circuit is identical to that shown in Figure 6b. F_o again is the frequency associated with the RC time constant:

$$F_o = \frac{1}{2\pi RC} \qquad \text{Eq. 6}$$

The frequency response of the system is extended to a frequency f_1 where

$$F_1 = A_o F_o \qquad \text{Eq. 7}$$

Note that the frequency response is automatically flat without having to match break points. However, the total bandwidth of the system (F_1) is still limited by the value of the shunt capacitance C across the input. This improved frequency response of the feedback technique avoids the use of low values for R which could generate excessive current noise.

b. Refinements of the Feedback System. A major difficulty of the feedback system arises from shunt capacitance associated with the high-megohm resistor R in the feedback path. If the shunt capacitance across the resistor is C_F, then the bandwidth (F_F) of the system is determined by the time constant RC_F:

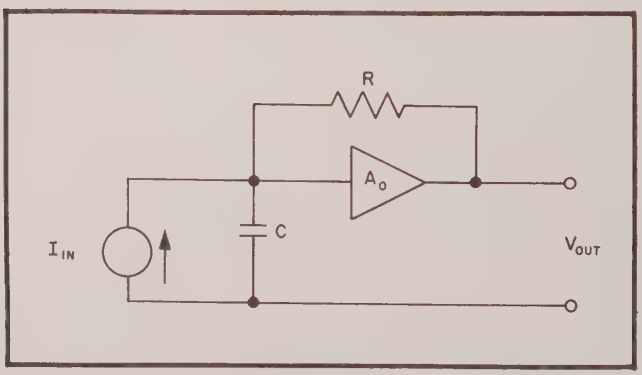


FIGURE 7. Basic circuit configuration for the feedback method.

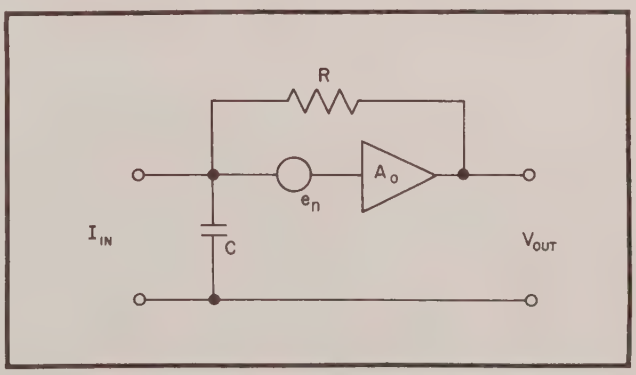


FIGURE 8. The voltage noise associated with the amplifier input device is an important source of noise in the high-speed feedback system.

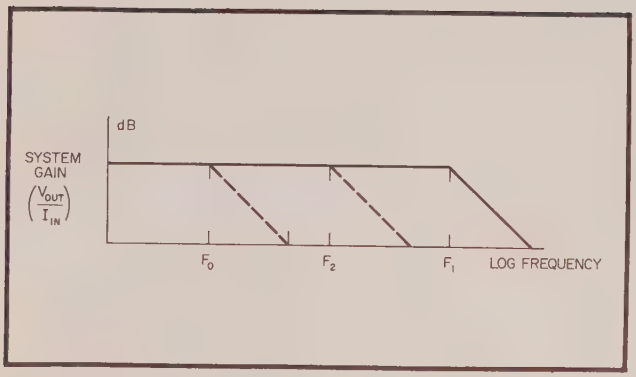


FIGURE 9. The bandwidth of the high-speed feedback system (Fig. 9a) can be limited by using a filter with either a -6 dB/octave or a -12 dB/octave roll-off. The effect of the filter on the noise spectrum is shown in Fig. 9b. Effect of input capacitance on noise is shown in Fig. 9c.

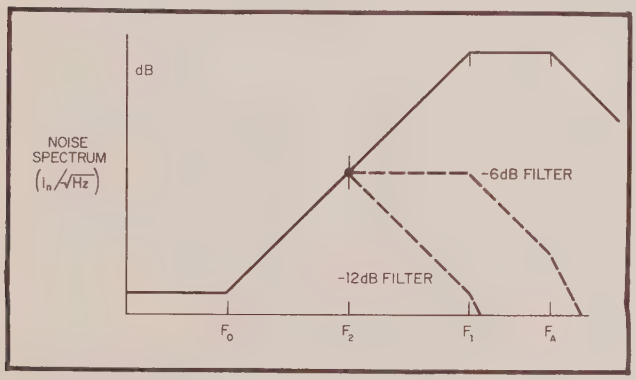


FIGURE 9b. Effect of filter on noise spectrum.

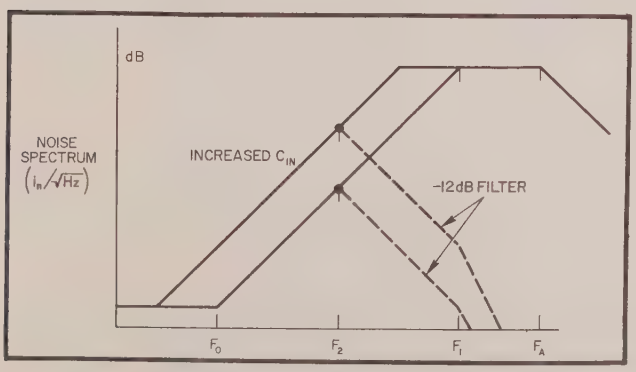


FIGURE 9c. Effect of input capacitance on noise.

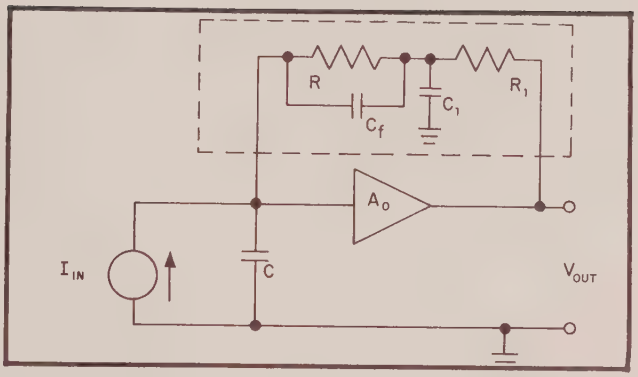


FIGURE 10. Frequency compensation.

$$F_F = \frac{1}{2\pi RC_F} \qquad \text{Eq. 8}$$

A slight modification of the feedback loop can correct this problem as shown in Figure 10. If the time constant R_1C_1 is made equal to the time constant $R \cdot C_F$, it can be shown that the circuit within the dotted line behaves exactly as a resistance R. The matching of time constants in this case does not become a drawback because the capacitances involved are all constant and not affected by input impedance.

c. -12 dB/octave Filter.

1. Theory. To obtain optimum wideband noise performance a filter with a single high-frequency roll-off (i.e., -6 dB/octave) is not sufficient and -12 dB/octave is required. The effect of a -6 dB filter is shown in Figure 9a and b. The filter is used to limit the system bandwidth to a frequency F_2, smaller than F_1. The effect of this filter on the noise spectrum is shown in Figure 9b. It can be seen that there are again high-frequency noise components above F_2, the useable bandwidth of the system. These can be eliminated by using a filter with a -12 dB/octave roll-off. The result of such a filter on noise performance is also shown in Figure 9b.

2. Model 427. The input amplifier is followed by an adjustable low-pass filter having a -12 dB/octave roll-off and a voltage gain of 10X. The voltage gain in the low-pass filter avoids premature overloading in the input amplifier which can be seen as follows. The maximum output voltage V_{out} is ± 10 volts. The maximum signal level at the input of the low-pass filter is, therefore, ± 1 volt. At this point in the circuit, wide-band noise could still be present and exceed the 1-Volt signal level. The voltage gain of 10 in the filter allows the total pre-filter wide-band noise to exceed the full scale signal by a factor of 10 (20 dB). The frequency response of this filter is adjustable for variable "damping" control.

2-3. CONNECTIONS.

a. Input. The input receptacle (J202) is a BNC type which mates with coaxial cables such as Keithley Models 8201 and 8202. The inner contact is circuit high. The outer shell is low or chassis ground.

b. Output. Two output receptacles are provided (J102 on the front, J103 on the rear panel). These are BNC types where the inner contact is output high and the outer shell is chassis ground.

c. Power Input. The power receptacle (P305) on the rear panel is a 3-prong connector which mates with Keithley part number CO-6 line cord.

2-4. CONTROLS.

a. Front Panel.

1. Power Switch "PUSH ON" (S302). This switch controls the line power to the instrument. The switch is a special pushbutton type with "Power On" indicated by a self-contained pilot lamp.

2. GAIN (VOLTS PER AMPERE) (S201). This switch sets the overall gain in eight positions from 10^4 to 10^{11}. A "ZERO CHECK" position permits adjustment of zero offsets.

3. RISE TIME Switch (S101). This switch sets the 10-90% rise time in 10 positions from .01 to 300 milliseconds (for the filter section only).

4. SUPPRESSION (MAX) Switch (S303). This switch sets the maximum current suppression in eight positions from 10^{-10} to 10^{-3} A. When the switch is set to "OFF" the current suppression circuit is disabled.

5. SUPPRESSION (FINE) Control (R333). This control permits adjustment of suppression with 0.1% resolution.

6. SUPPRESSION (POLARITY) Switch (S304). This switch sets the polarity of the current suppression (referred to the input).

7. ZERO ADJUST Control (R235). This control permits adjustment of zero offset through the use of the OVERLOAD indicator.

b. Rear Panel.

1. Line Voltage Switch (S301). Sets instrument for either 117 or 234 V operation.

2-5. OPERATING CONSIDERATIONS.

a. Gain. The gain of the Model 427 is defined in terms of volts per ampere. Since the output level is 10 volts for a full scale input, the gain could also be expressed as sensitivity in amperes referred to the input as in Table 2-1. $V_{out} = -(I_{in} \times GAIN)$ Eq. 9

TABLE 2-1.
Gain or Sensitivity Referred to the Input

GAIN Setting	Feedback Resistor	Full Scale Sensitivity (Amperes)	Full Scale Output (Volts)
10^4	10^3	1×10^{-3}	10
10^5	10^4	1×10^{-4}	10
10^6	10^5	1×10^{-5}	10
10^7	10^6	1×10^{-6}	10
10^8	10^7	1×10^{-7}	10
10^9	10^8	1×10^{-8}	10
10^{10}	10^9	1×10^{-9}	10
10^{11}	10^{10}	1×10^{-10}	10

b. Rise Time. The rise time for each gain setting is listed in the specifications as "FAST RISE TIME". These rise times are obtained when the RISE TIME switch is set to the positions indicated in Table 2-2.

TABLE 2-2.
Switch Settings for "FAST RISE TIME"

GAIN Setting	Rise Time	RISE TIME Settings	Dynamic Range
10^4	15 µs	.01 ms	2000
10^5	15 µs	.01 ms	2000
10^6	15 µs	.01 ms	2000
10^7	40 µs	.03 ms	2000
10^8	60 µs	.03 ms	800
10^9	220 µs	.1 ms	400
10^{10}	400 µs	.3 ms	200
10^{11}	1.5 ms	1 ms	100

c. Suppression. Current suppression is provided in the Model 427 for suppression of input currents up to 10^{-3} amperes. By suppressing background currents, small variations in a larger signal can be observed. Currents of either polarity can be suppressed. To suppress an input current the SUPPRESSION should be set to supply a current of opposite polarity. The FINE control permits adjustment up to 1.5 times the MAX setting.

d. Overloads. The overload sensing circuit detects an overload at two places in the circuit: before and after the "RISE TIME" filter circuit. The OVERLOAD lamp (DS302) will indicate whenever the voltage sensed is greater than full scale regardless of the RISE TIME setting or the frequency.

e. Zero Adjust. The ZERO CHECK position grounds the the input of the instrument and converts the current amplifier to a high-gain voltage amplifier. The amplified offset voltage will turn on the OVERLOAD indicator whenever the input voltage offset exceeds ±100 µV. Therefore the ZERO control should be adjusted so that the OVERLOAD indicator is off when in ZERO CHECK mode, yielding the specified input voltage drop.

SECTION 3. APPLICATIONS

3-1. CURRENT MEASURING SYSTEM. The typical current measuring system consists of a current source, a current amplifier, and a monitoring device. The current source could include an ion chamber, photomultiplier, or other high-impedance device. The current amplifier such as the Model 427 provides sufficient gain to drive a monitoring device such as a chart recorder or other readout. The Model 427 in this case provides an output voltage which is calibrated in volts per ampere as in equation 10.

$$I_{in} = - (V_{out} / GAIN) \qquad \text{Eq. 10}$$

Example:

GAIN = 10^6 volts/ampere

V_{out} = +500 mV

The input current I_{in} would be:

$I_{in} = - (5 \times 10^{-1} \text{volts} / 10^6 \text{volts per ampere})$

$I_{in} = - 5 \times 10^{-7}$ amperes

3-2. NOISE BANDWIDTH CONSIDERATIONS. Table 3-1 illustrates the trade-off between fast rise time and dynamic range. For this application dynamic range is defined as the ratio of maximum peak-to-peak current to peak-to-peak current noise. Peak-to-peak current noise is taken as 5-times the rms current noise. The maximum peak-to-peak current is 2-times the maximum full scale current.

NOTE

When using current suppression the current-suppression resistor should be considered as an additional current-noise generator. The values given in Table 3-1 do not include the contribution of the suppression resistor. Therefore the selected suppression resistor R_S, should be as large as possible to minimize the contribution to current noise.

3-3. NOISE-IMPROVEMENT CONTOURS. The sensitivity and speed of the Model 427 (for either d-c or a-c measurements) can be compared to the best performance obtainable with the shunt method of measuring current. The best "noise-risetime" product that can be achieved for d-c measurements (with 100 pF shunt capacitance) in a shunt system is 7 x 10^{-15} ampere-seconds. However the feedback system achieves 2 x 10^{-15} ampere-seconds (also with 100 pF shunt capacitance). When used in a-c narrowband systems (lock-in, etc.) the degree of improvement is a function of shunt capacitance and operating frequency. The achieveable improvement over the shunt method can be plotted in a graph similar to a set of noise contours. Figure 11 shows the measured improvement (negative dB) that can be obtained with the Model 427 at a given frequency and shunt capacitance when compared to an ideal (noiseless) amplifier in a shunt system.

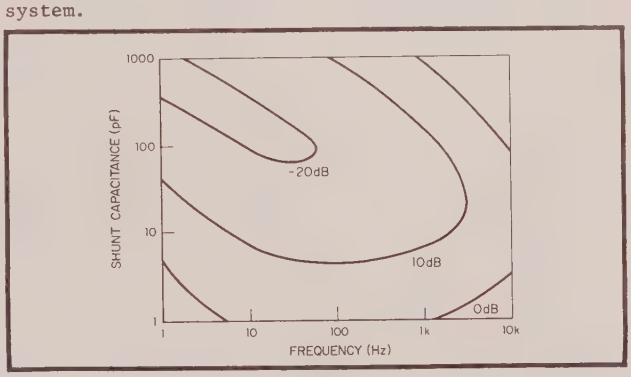


FIGURE 11. Plot of noise-improvement contours.

TABLE 3-1.
RMS Noise Current (Typical)[1] as a Function of Gain and Rise-Time Setting

GAIN	MAXIMUM FULL SCALE CURRENT	RISE TIME SETTING									
V/A	AMPERES	300	100	30	10	3	1	.3	.1	.03	.01
10^4	10^{-3}	*	*	*	*	*	*	1×10^{-8}	1.2×10^{-8}	4×10^{-8}	1×10^{-7}
10^5	10^{-4}	*	*	*	*	*	*	1×10^{-9}	1.2×10^{-9}	4×10^{-9}	1×10^{-8}
10^6	10^{-5}	*	*	*	*	*	*	1×10^{-10}	1.2×10^{-10}	4×10^{-10}	1×10^{-9}
10^7	10^{-6}	*	*	*	*	*	1×10^{-11}	1.5×10^{-11}	2×10^{-11}	1×10^{-10}	x
10^8	10^{-7}	*	*	*	*	1×10^{-12}	2×10^{-12}	5×10^{-12}	1×10^{-11}	4×10^{-11}	x
10^9	10^{-8}	*	*	*	2×10^{-13}	2×10^{-13}	5×10^{-13}	2×10^{-12}	5×10^{-12}	x	x
10^{10}	10^{-9}	*	1×10^{-14}	2×10^{-14}	5×10^{-14}	2×10^{-13}	5×10^{-13}	2×10^{-12}	x	x	x
10^{11}	10^{-10}	2×10^{-15}	4×10^{-15}	1×10^{-14}	4×10^{-14}	1×10^{-13}	4×10^{-13}	x	x	x	x

[1] With up to 100 pF input shunt capacitance. Noise increases as input shunt capacitance increases.

KEY:
x = Filter Bandwidth is greater than current-amplifier bandwidth.
* = Larger Rise Times are useful for increased filtering of the signal and noise inherent in the source. They do not further improve the instrument noise contribution except when the input shunt capacitance exceeds 100 pF.

SECTION 4. ACCESSORIES

4-1. GENERAL. The following Keithley accessories can be used with the Model 427 to provide additional convenience and versatility.

4-2. OPERATING INSTRUCTIONS. A separate Instruction Manual is supplied with each accessory giving complete operating information.

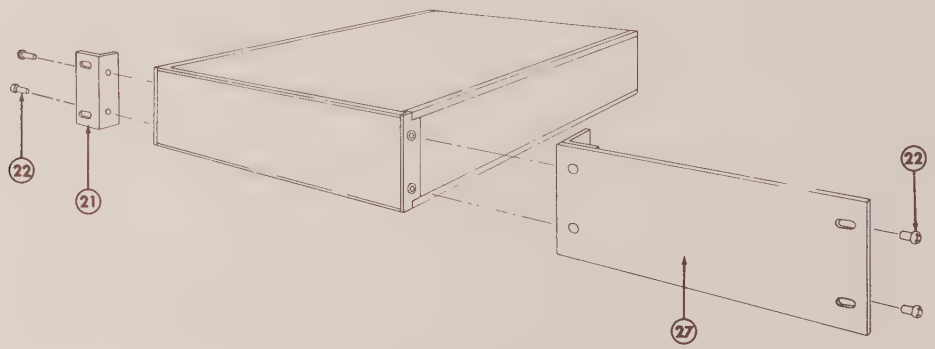
Model 2000 Rack Mounting Kit

Description:

The Model 2000 is a rack mounting kit which converts any half-rack, Style M instrument from bench mounting to rack mounting in a standard 19-inch rack. The dimensions are 3-1/2" high x 19" wide. The hardware included in this kit consists of a blank panel which can be mounted on either side of a half-rack instrument.

Parts List:

Item No.		Qty. Req'd	Keithley Part No.
21	Angle Bracket	1	24783A
22	Screws, #6-32 x 5/8, Phillips	4	-
27	Staked Panel	1	250048



Models 8201, 8202 Coaxial Cables

Description:

These cables are coaxial types with BNC connectors on each end. The Model 8201 cable is 10 inches long while the Model 8202 is 20 inches.

Application:

These cables mate with the BNC receptacles on the 427.

Model 1007 Dual Rack Mounting Kit

Description:

The Model 1007 is dual rack mounting kit with overall dimensions 3-1/2" high and 19" wide. The hardware included in this kit consists of two Angle Brackets, one Mounting Clamp and extra mounting screws.

Application:

The Model 1007 converts any half-rack, style M instrument from bench mounting to rack mounting in a standard 19-inch rack.

Installation:

a. Before assembling the rack kit, determine the position of each instrument. Since the instruments can be mounted in either location, their position should be determined by the user's measurement. The following instructions refer to instruments "A" and "B" positioned as shown.

b. Once the position of each instrument has been determined, the "side dress" panels (Item 11) on adjacent sides should be removed. Removal is accomplished by loosening the socket head screws (Item 24) in two places. Slide the "side dress" panels to the rear of the instrument to remove.

c. The "mounting clamp" (Item 23) is installed on instrument "A" using the original hardware (Item 24). With the socket head screws removed, insert the "mounting clamp" behind the "corner bracket"(Item 7) and replace the screws to hold the mounting clamp in place.

Parts List:

Item No.	Description	Qty. Req'd	Keithley Part No.
21	Angle Bracket	2	24783A
22	Screw, #6-32 x 5/8, Phillips	4	-
23	Mounting Clamp	1	24798B
24	Screw, #6-32 x 1/2, FH Socket (Original hardware)	4	-
25	Screw, #6-32 x 1-1/8, Phillips	1	-
26	Kep Nut, #6-32	1	-

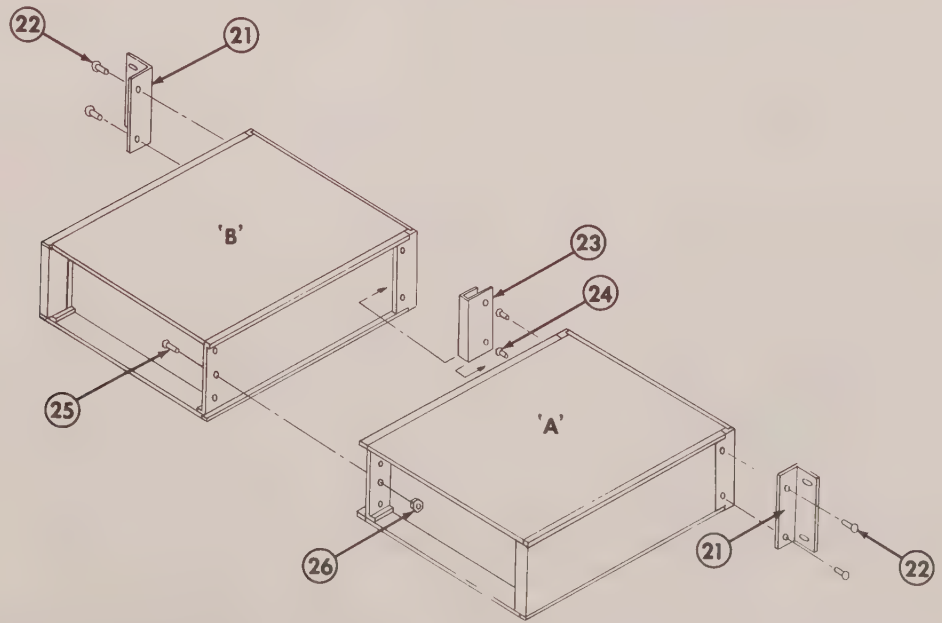
d. Tighten the socket head screws (Item 24) on instrument "B". Insert the "mounting clamp" behind the "corner bracket" on instrument "B" as shown.

e. When mounting instruments having the same depth, a screw (Item 24) and kep nut (Item 26) are required to secure the two instruments together.

f. Attach an "angle bracket" (Item 21) on each instrument using hardware (Item 22) in place of the original hardware (Item 24).

g. The bottom cover feet and tilt bail assemblies may be removed if necessary.

h. The original hardware, side dress panels, feet and tilt bail assemblies should be retained for future conversion back to bench mounting.



SECTION 5. CIRCUIT DESCRIPTION

5-1. GENERAL. The Model 427 is composed of a feedback amplifier, a X10 gain filter section, suppression and power supply circuits as shown in Figure 12. The feedback amplifier is located on the "Amplifier Board", PC-289. The filter circuitry is located on the "Filter Board", PC-291, PC-292. The power supply circuitry is located on the "Mother Board", PC-290.

5-2. FEEDBACK AMPLIFIER (PC-289). The feedback amplifier is composed of a high-gain amplifier connected as a feedback ammeter. The feedback resistors R220 through R227 are set by the GAIN Switch (S201). The high-gain amplifier is composed of a dual FET input stage (Q201A and B), a differential amplifier (QA201), and an output stage (Q203 and Q204). The feedback is connected from resistor R201 to the output stage at Q203 and Q204. Potentiometers R232, R233, and R234 are internal frequency compensation controls for 10^9, 10^{10}, and 10^{11} gains respectively. Potentiometer R235 is the ZERO ADJ control. The full scale output of the feedback amplifier is 1 volt.

5-3. FILTER (PC-292). The filter circuit is composed of a high-gain amplifier connected as a 12 dB/octave low pass filter as shown in Figure 13. The amplifier consists of integrated circuit QA101 and output stage (Q101 and Q102). Full scale output is 10 volts. The gain is established at X10 by resistors R110 and R112 + R113. Potentiometer R108 is an internal zero adjustment. Potentiometer R113 is an internal gain adjustment.

5-4. POWER SUPPLY (PC-290). The power supply provides ±15 V dc at up to 70 mA for the amplifier circuits. The regulator circuits are composed of identical components and are connected as shown in Figure 14.

a. +15 V Regulator. AC power is tapped from one secondary of transformer T301. The ac is rectified by a full-wave bridge rectifier (D301). Transistor Q301 is the series pass regulator. Integrated circuit QA 301 is a self-contained reference and regulating circuit. Potentiometer R304 is an internal voltage adjustment. Resistor R307 serves as a current limit device.

b. -15 V Regulator. AC power is tapped from one secondary of transformer T301. The ac is rectified by a full-wave bridge rectifier (D302). Transistor Q302 is the series pass regulator. Integrated circuit QA-302 is a self-contained reference and regulating circuit. Potentiometer R309 is an internal voltage adjustment. Resistor R307 serves as a current limit device.

5-5. CURRENT SUPPRESSION CIRCUITRY (PC-290). The suppression is applied at the input as shown in Figure 15. The MAX AMPERES Switch (S303) sets the current suppression in decade steps from 10^{-3} to 10^{-10} amperes (Resistors R325 through R332). Potentiometer R333 is the FINE Control which provides adjustment from 0 to 1.5 times the MAX setting. Switch S304 sets the polarity (either + and - 15 volt source). Current suppression is a function of V_{CS}/R_{CS},

where V_{CS} = Voltage at the wiper of R333.

R_{CS} = Series Resistor (R325 through R332).

Example: If MAX AMPERES = 10^{-6}

and if V_{CS} = +15 V

then $I_{CS} = \frac{+15V}{10^7\Omega} = +1.5 \times 10^{-6}$ amperes

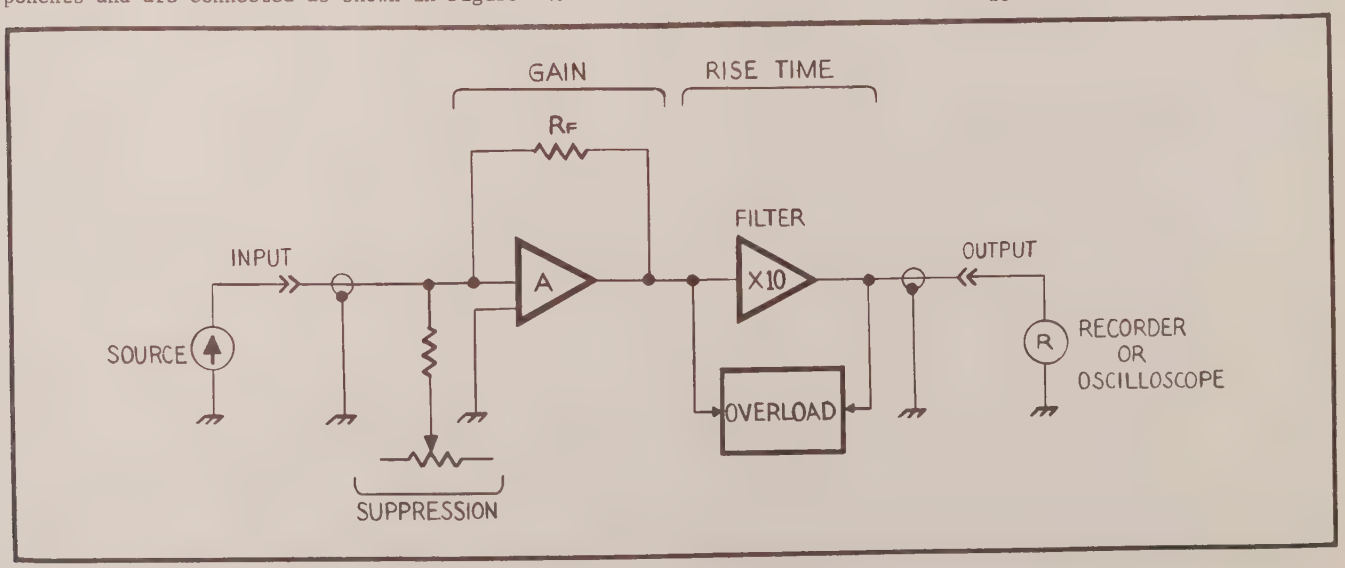


FIGURE 12. Block diagram of a high-speed current amplifier

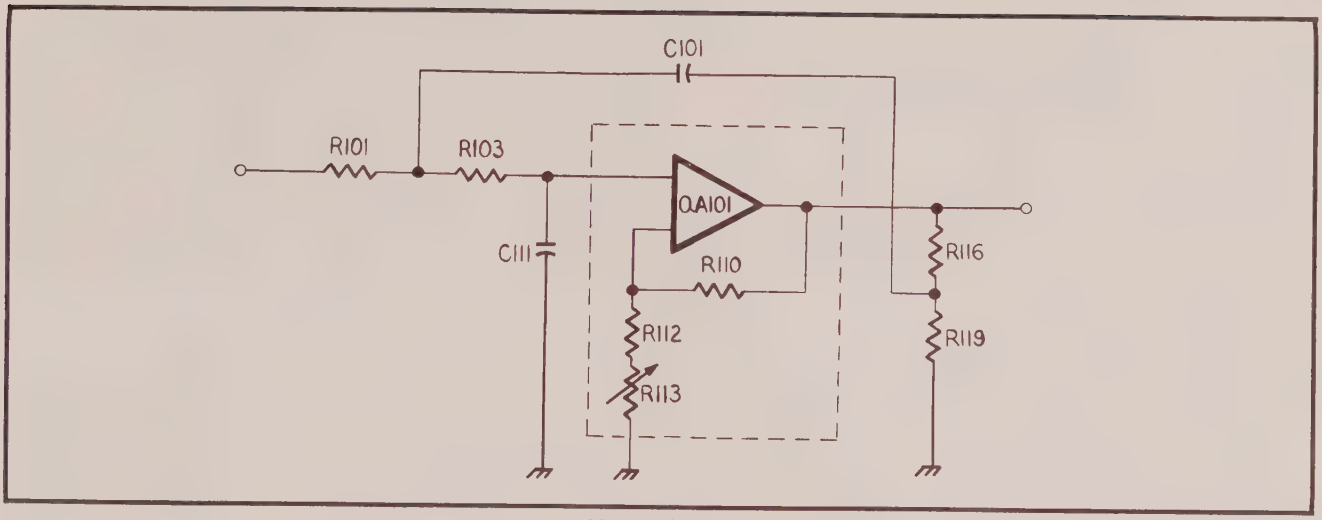


FIGURE 13. Filter Circuit.

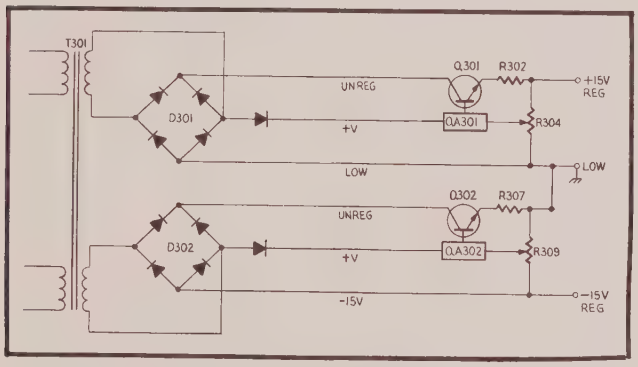


FIGURE 14. Power Supply Regulator.

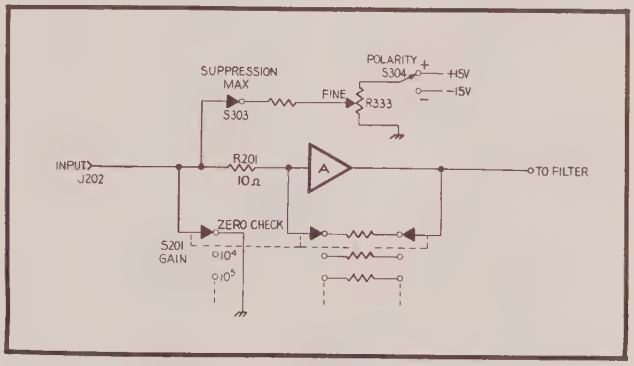


FIGURE 15. Current Suppression.

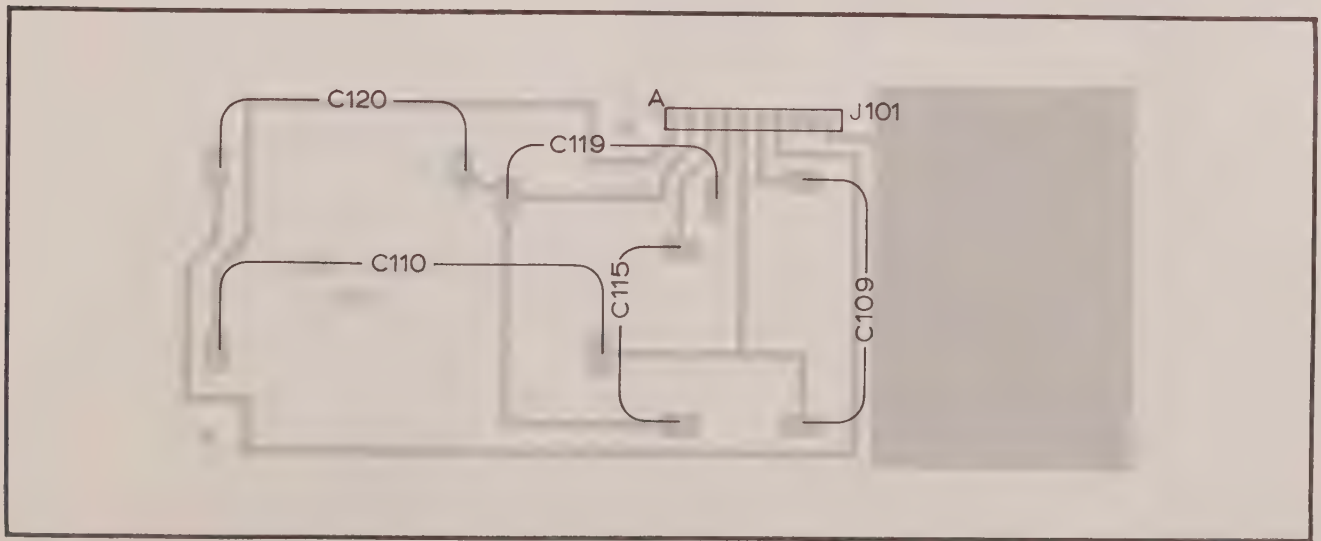


FIGURE 16. Component Layout - PC-291.

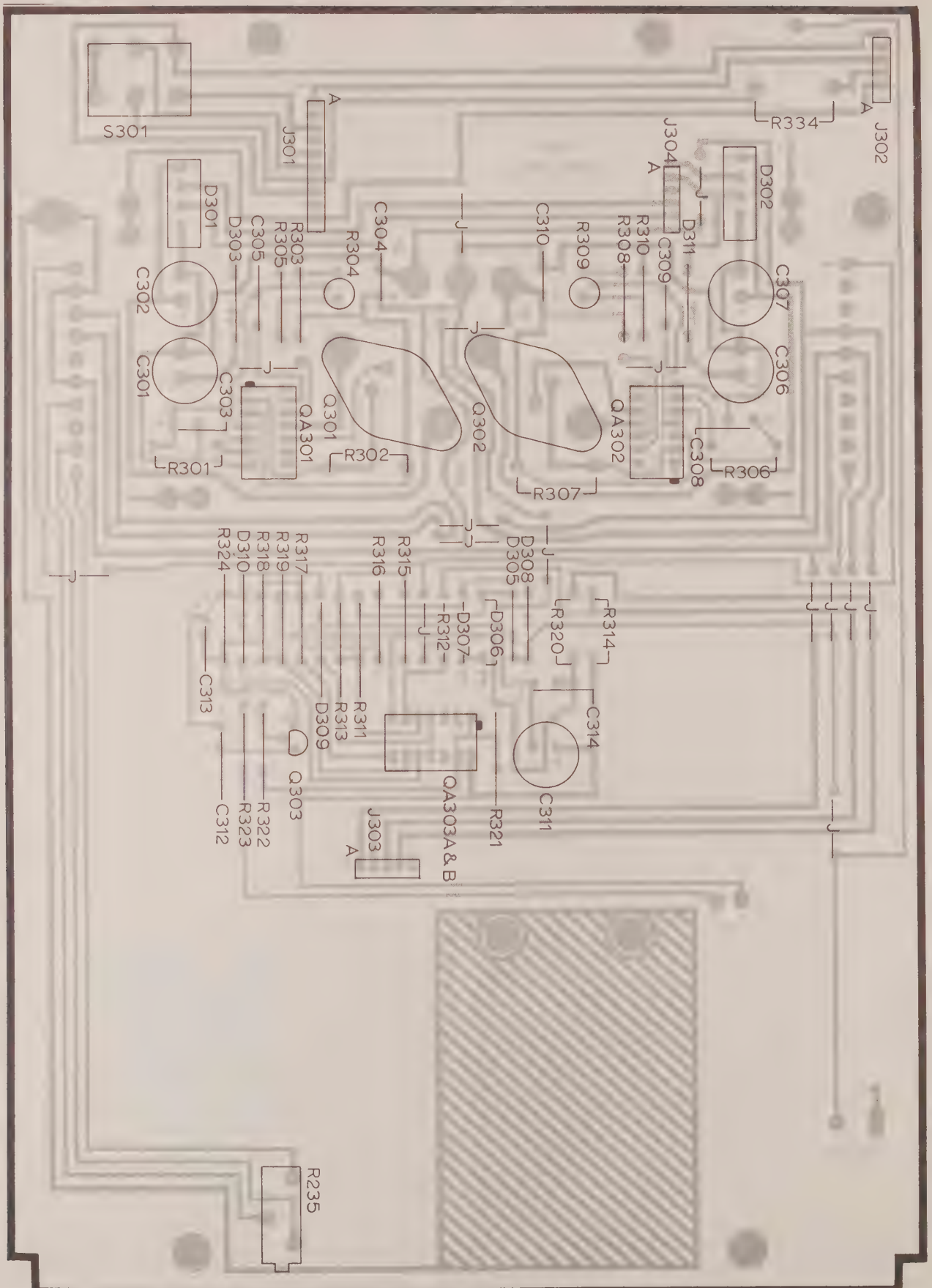


FIGURE 17. Component Layout - PC-290.

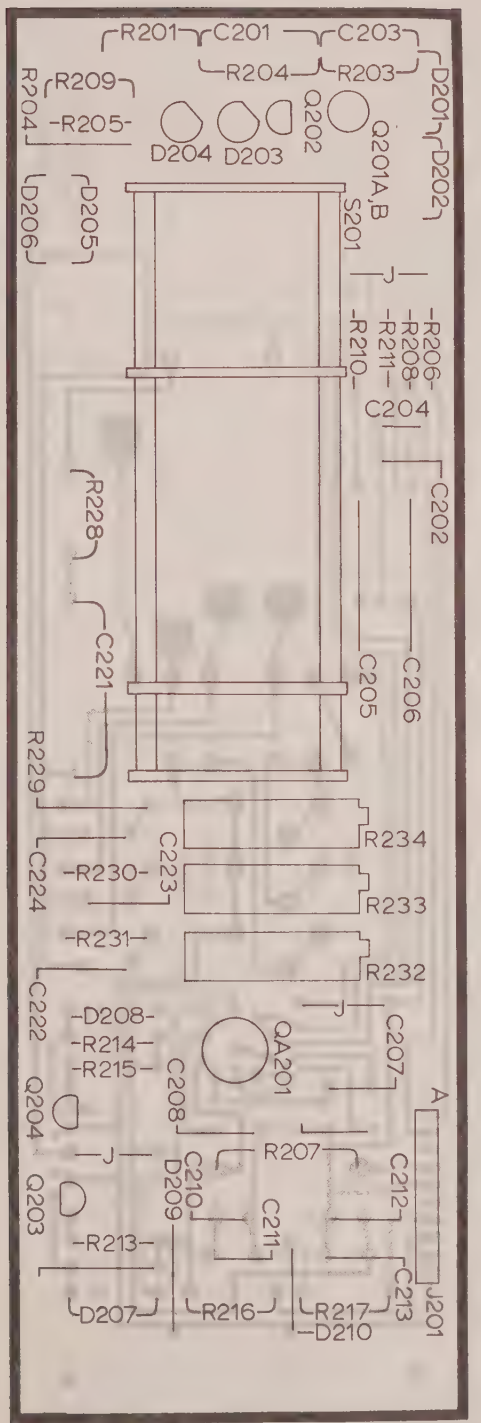


FIGURE 18.
Component Layout - PC-289.

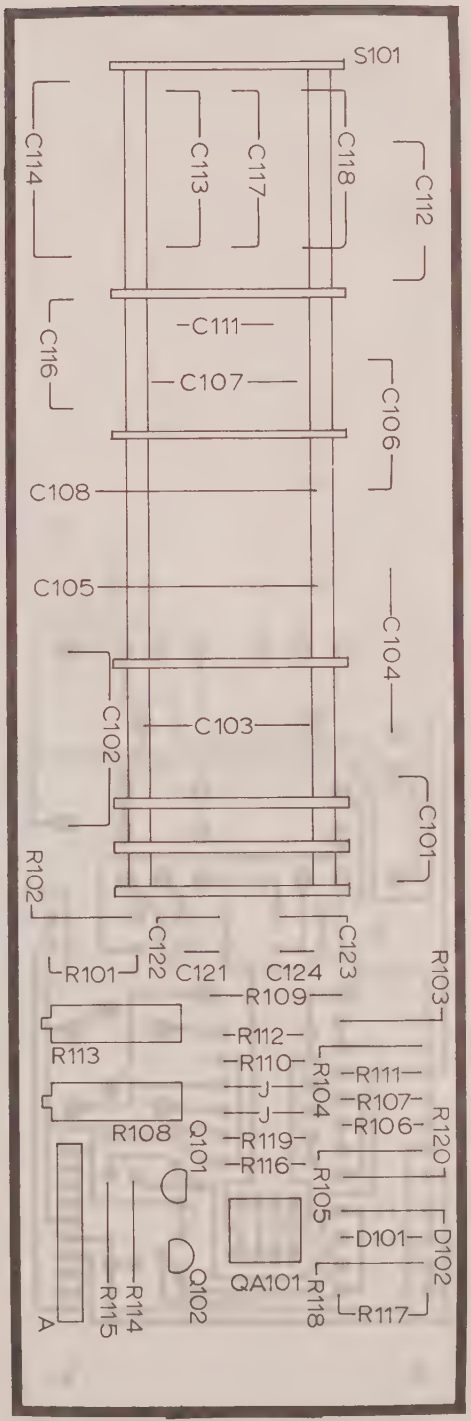


FIGURE 19.
Component Layout - PC-292.

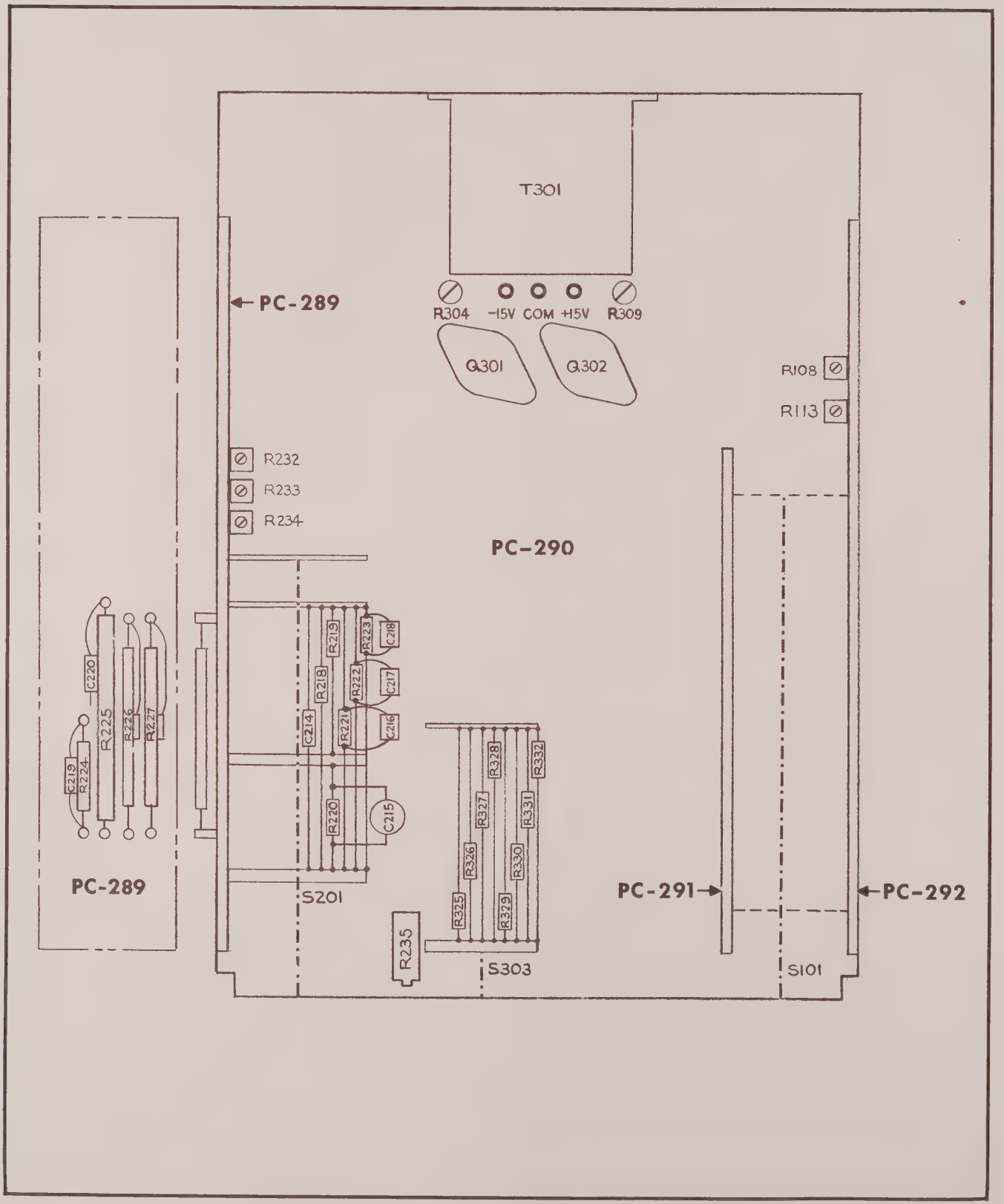


FIGURE 20. Chassis - Top View.

SECTION 6. REPLACEABLE PARTS

6-1. REPLACEABLE PARTS LIST: This section contains a list of components used in this instrument for user reference. The Replaceable Parts List describes the individual parts giving Circuit Designation, Description, Suggested Manufacturer (Code Number), Manufacturer's Part Number, and the Keithley Part Number. Also included is a Figure Reference Number where applicable. The complete name and address of each Manufacturer is listed in the CODE-TO-NAME Listing following the parts list.

TABLE 6-1.
Abbreviations and Symbols

A	ampere	F	farad	Ω	ohm
		Fig	Figure		
CbVar	Carbon Variable			p	pico (10^{-12})
CerD	Ceramic Disc	GCb	Glass enclosed Carbon	PC	Printed Circuit
CerTB	Ceramic Tubular			Poly	Polystyrene
Cer Trimmer	Ceramic Trimmer	k	kilo (10^{3})		
Comp	Composition			Ref.	Reference
		μ	micro (10^{-6})		
DCb	Deposited Carbon			TCu	Tinner Copperweld
Desig.	Designation	M	Meg (10^{6})		
		Mfr.	Manufacturer	V	volt
EAL	Electrolytic, Aluminum	MtF	Metal Film		
ETB	Electrolytic, Tubular	My	Mylar	W	watt
ETT	Electrolytic, Tantalum			WW	Wirewound
		No.	Number	WWVar	Wirewound Variable

6-2. ELECTRICAL SCHEMATICS AND DIAGRAMS. Schematics and diagrams are included to describe the electrical circuits as discussed in Section 5. Table 6-2 identifies all schematic part numbers included.

6-3. HOW TO USE THE REPLACEABLE PARTS LIST. This Parts List is arranged such that the individual types of components are listed in alphabetical order. Main Chassis parts are listed followed by printed circuit boards and other subassemblies.

6-4. HOW TO ORDER PARTS.

a. Replaceable parts may be ordered through the Sales Service Department, Keithley Instruments, Inc. or your nearest Keithley representative.

b. When ordering parts, include the following information.

1. Instrument Model Number
2. Instrument Serial Number
3. Part Description
4. Schematic Circuit Designation
5. Keithley Part Number

c. All parts listed are maintained in Keithley Spare Parts Stock. Any part not listed can be made available upon request. Parts identified by the Keithley Manufacturing Code Number 80164 should be ordered directly from Keithley Instruments, Inc.

TABLE 6-2.
Electrical Schematics and Diagrams

Description	Circuit Designation	Schematic
Amplifier Board	PC-289	24766D
Mother Board (Power Supply)	PC-290	24768D
Filter Board	PC-291, PC-292	24767D

TABLE 6-3.
PC Board Designation Series

Series	Description	Designation	Page No.
100	Filter Circuit	PC-291	20
100	Filter Circuit	PC-292	20
200	Amplifier	PC-289	21
300	Power Supply	PC-290	23
300	Suppression Circuit	PC-290	23
300	Overload Circuit	PC-290	23

TABLE 6-4.
Mechanical Parts List

Item No.	Description	Qty. Per Assembly	Keithley Part No.	Figure No.
-	Chassis Assembly	-	-	21
-	Front Panel Assembly	-	-	
1	Front Panel	1	24756C	
2	Screw, Slotted, 6-32 x 3/8	4	-	
3	Front Panel Overlay	1	24758B	
4	Rear Panel	1	24760B	
5	Side Extrusion Left	1	24754C	
6	Side Extrusion Right	1	24754C	
7	Corner Bracket	2	24745B	
8	Screw, Socket, 6-32 x 1/4	4	-	
9	Screw, Phillips, 6-32 x 1/4	4	-	
10	Clip for Side Dress	2	FA-101	
11	Side Dress Panel	2	24755B	
-	Top Cover Assembly	-	-	
12	Top Cover	1	24732C	
13	Screw, Socket, 6-32 x 5/16	4	-	
-	Bottom Cover Assembly	-	24763B	22
14	Bottom Cover	1	24733C	
15	Screw, Socket, 6-32 x 5/16	4	-	
-	Feet Assembly	-	-	
16	Feet	4	24322B	
17	Ball	4	FE-6	
18	Tilt Bail	1	17147B	
19	Screw, Phillips, 6-32	4	-	
20	Kep Nut, 6-32	4	-	

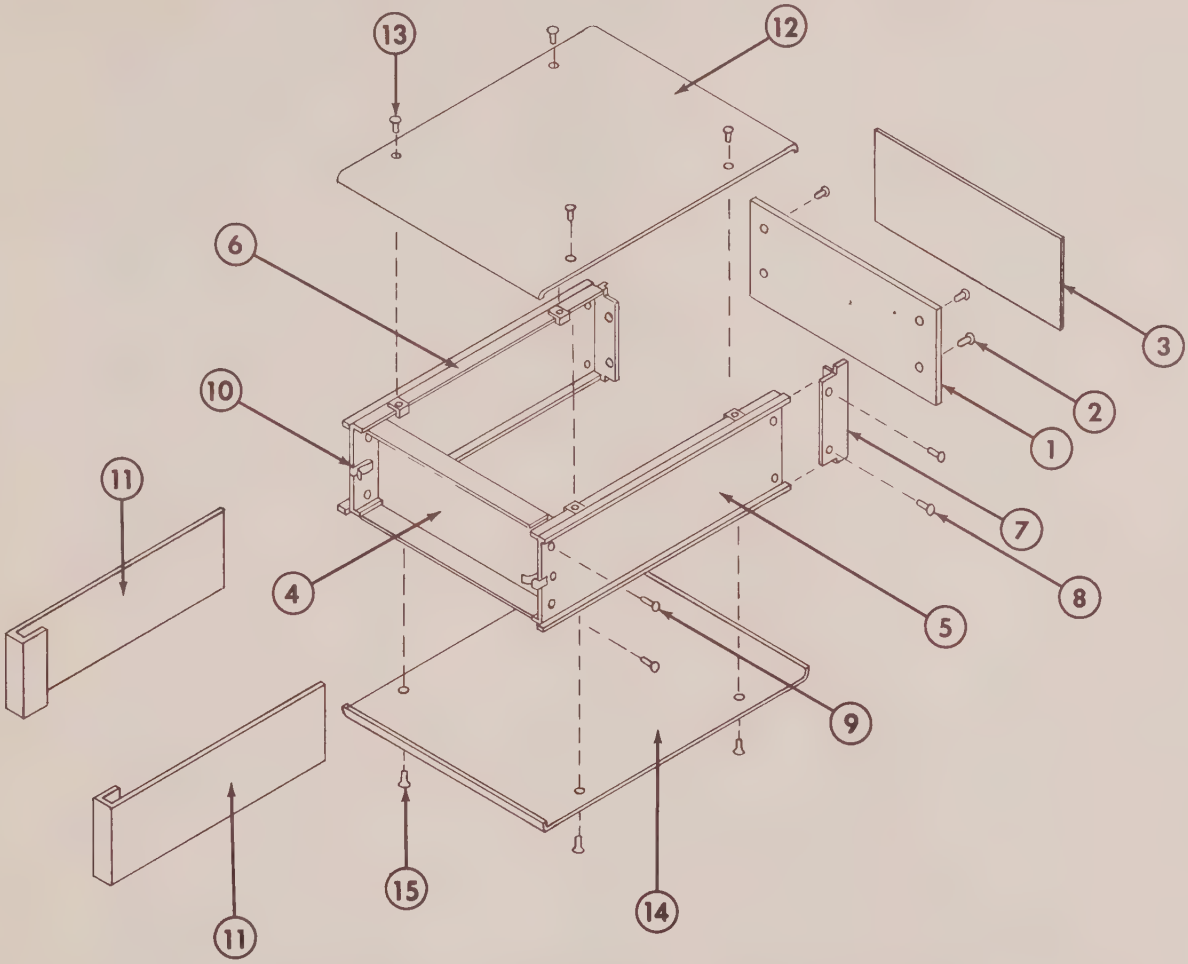


FIGURE 21. Chassis Assembly- Exploded View.

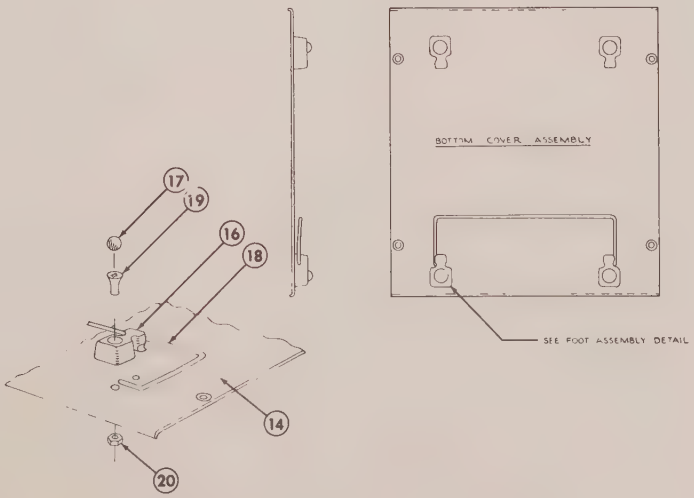


FIGURE 22. Bottom Cover Assembly.

FILTER BOARD
("100" SERIES, PC-291*, PC-292)

CAPACITORS

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
C101	150 pF	500 V	Poly	71590	CPR	C138-150P	19
C102	680 pF	500 V	Poly	71590	CPR	C138-680P	19
C103	.0022 µF	500 V	Poly	71590	CPR	C138-.0022M	19
C104	6800 pF	500 V	Poly	71590	CPR	C138-6800P	19
C105	.022 µF	200 V	Poly	84171	2PJ	C108-.022M	19
C106	.068 µF	100 V	My	88480	3FR	C146-.068M	19
C107	.22 µF	200 V	My	13050	5M1A	C47-.22M	19
C108	.68 µF	200 V	My	13050	5M1A	C47-.68M	19
C109*	2.2 µF	200 V	My	13050	5M1A	C47-2.2M	16
C110*	6.8 µF	200 V	My	97419	M2WF	C203-6.8M	16
C111	68 pF	500 V	Poly	71590	CPR	C138-68P	19
C112	330 pF	500 V	Poly	71590	CPR	C138-330P	19
C113	.001 µF	500 V	Poly	71590	CPR	C138-.001M	19
C114	.0033 µF	500 V	Poly	71590	CPR	C138-.0033M	19
C115*	.01 µF	200 V	Poly	84171	2PJ	C108-.01M	16
C116	.033 µF	100 V	My	88480	3FR	C146-.033M	19
C117	.1 µF	200 V	My	13050	SM1A	C47-.1M	19
C118	.33 µF	200 V	My	13050	SM1A	C47-.33M	19
C119*	1 µF	200 V	My	13050	SM1A	C47-1M	16
C120*	3.3 µF	200 V	My	13050	SM1A	C47-3.3M	16
C121	5 pF	1000 V	CerD	72982	-	C64-5P	19
C122	5 pF	1000 V	CerD	72982	-	C64-5P	19
C123	33 pF	1000 V	CerD	72982	-	C64-33P	19
C124	100 pF	100 V	CerD	72982	-	C64-100P	19

MISCELLANEOUS

Circuit Desig.	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
J101	Connector, 10-Pin, Mini-PV	22526	20052	CS-237	19
QA101	Integrated Circuit	12040	LM301AN	IC-24	19
D101	Diode, Rectifier	01295	1N914	RF-28	19
D102	Diode, Rectifier	01295	1N914	RF-28	19
Q101	Transistor	04713	2N3903	TG-49	19
Q102	Transistor	04713	2N3905	TG-53	19
S101	Switch, Rotary, RISE TIME	-	-	SW-338	19
J102	Connector, BNC	95712	6672NT34	CS-15	3

RESISTORS

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
R101	7.78 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-7.78k	19
R102	8.41 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-8.41k	19
R103	51.7 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-51.7k	19
R104	51.7 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-51.7k	19
R105	~~14.7~~ kΩ 10 KΩ	1%, 1/8 W	MtF	07716	CEA	R88-~~14.7k~~ -10K	19

RESISTORS (cont'd)

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
R106	1 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1k	19
R107	1 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1k	19
R108	200 Ω	.75 W	Comp	80294	3009P	RP-89-200	19
R109	1 MΩ	.1%, 1/2 W	MtF	91637	MFF	R169-1M	19
R110	536 kΩ	.1%, 1/2 W	MtF	91637	MFF	R168-536k	19
R111	1 kΩ	10%, 1/4 W	Comp	44655	RC07	R76-1k	19
R112	61.9 kΩ	.1%, 1/8 W	MtF	91637	MFF	R168-61.9k	19
R113	2 kΩ	.75 W	Comp	80294	3009P	RP-89-2k	19
R114	10 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-10k	19
R115	470 Ω	10%, 1/4 W	Comp	44655	RC07	R76-470	19
R116	1.8 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1.8k	19
R117	10 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-10k	19
R118	470 Ω	10%, 1/8 W	Comp	44655	RC07	R76-470	19
R119	200 Ω	1%, 1/8 W	MtF	07716	CEA	R88-200	19
R120	14.7 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-14.7k	19

AMPLIFIER BOARD
("200" SERIES, PC-289)

CAPACITORS (* Located on Switch S201.)

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
C201	.0022 µF	600 V	CerD	72982	ED	C22-.0022M	18
C202	.001 µF	1000 V	CerD	72982	-	C64-.001M	18
C203	1.5 pF	600 V	CerT	71590	TCZ-1R5	C77-1.5P	18
C204	.001 µF	1000 V	CerD	72982	-	C64-.001M	18
C205	.047 µF	200 V	My	13050	SM2A	C143-.047M	18
C206	.047 µF	200 V	My	13050	SM2A	C143-.047M	18
C207	470 pF	1000 V	CerD	72982	-	C64-470P	18
C208	.0022 µF	600 V	CerD	72982	ED	C22-.0022M	18
C209	.001 µF	1000 V	CerD	72982	-	C64-.001M	18
C210	10 µF	20 V	ETT	17554	TSD1-20	C179-10M	18
C211	.001 µF	1000 V	CerD	72982	-	C64-.001M	18
C212	10 µF	20 V	ETT	17554	TSD1-20	C179-10M	18
C213	.001 µF	1000 V	CerD	72982	-	C64-.001M	18
* C214	.0047 µF	200 V	MMT	97419	-	C66-.0047M	20
* C215	.0022 µF	600 V	CerD	72982	ED	C22-.0022M	20
* C216	470 pF	500 V	Poly	71590	CPR	C138-470P	20
* C217	47 pF	500 V	Poly	71590	CPR	C138-47P	20
* C218	5 pF	200 V	Poly	00686	E1013-1	C31-5P	20
C219	1.5 pF	600 V	CerT	71590	TCZ-1R5	C77-1.5P	20
C220	1.5 pF	600 V	CerT	71590	TCZ-1R5	C77-1.5P	20
C221	.033 µF	100 V	My	88480	3FR	C146-.003M	18
C222	.001 µF	1000 V	CerD	72982	-	C64-.001M	18
C223	47 pF	1000 V	CerD	72982	-	C64-47P	18
C224	.0033 µF	600 V	CerD	72982	ED	C22-.0033M	18

DIODES

Circuit Desig.	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
D201	Special	80164	-	RF-24555A	18
D202	Special	80164	-	RF-24555A	18
D203	Silicon	07263	2N3565	TG-39	18
D204	Silicon	07263	2N3565	TG-39	18
D205	-	01295	1N645	RF-14	18
D206	-	01295	1N645	RF-14	18
D207	Silicon	01295	1N914	RF-28	18
D208	Silicon	01295	1N914	RF-28	18
D209	Silicon	01295	1N914	RF-28	18
D210	Silicon	01295	1N914	RF-28	18

MISCELLANEOUS

Circuit Desig.	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
QA201	Integrated Circuit, Operational Amplifier	07263	μA715C	IC-26	18
S201	Switch, Rotary, GAIN	-	-	SW-337	18
J201	Connector	95712	6672NT34	CS-15	18

RESISTORS (* Located on Switch S201.)

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
R201	10 Ω	10%, 1/4 W	Comp	44655	RC07	R76-10	18
R202	1 MΩ	10%, 1/2 W	Comp	01121	EB	R1-1M	18
R203	100 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-100k	18
R204	23.2 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-23.2k	18
R205	22.1 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-22.1k	18
R206	10 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-10k	18
R207	18.2 kΩ	1%, 1/2 W	MtF	07716	CEC	R94-18.2k	18
R208	10 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-10k	18
R209	12.1 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-12.1k	18
R210	499 Ω	1%, 1/8 W	MtF	07716	CEA	R88-499	18
R211	499 Ω	1%, 1/8 W	MtF	07716	CEA	R88-499	18
R212	10 Ω	1%, 1/8 W	MtF	07716	CEA	R88-10	18
R213	470 Ω	10%, 1/4 W	Comp	44655	RC07	R76-470	18
R214	10 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-10k	18
R215	470 Ω	10%, 1/4 W	Comp	44655	RC07	R76-470	18
R216	10 Ω	10%, 1/4 W	Comp	44655	RC07	R76-10	18
R217	10 Ω	10%, 1/4 W	Comp	44655	RC07	R76-10	18
* R218	270 kΩ	10%, 1/2 W	Comp	01121	EB	R1-270k	20
* R219	100 Ω	1%, 1/2 W	MtF	07716	CEC	R94-100	20
* R220	900 Ω	1%, 1/2 W	DCb	91637	DCF-1/2	R12-900	20
* R221	10 kΩ	1%, 1/2 W	MtF	07716	CEC	R94-10k	20
* R222	100 kΩ	1%, 1/2 W	MtF	07716	CEC	R94-100k	20
* R223	1 MΩ	1%, 1/2 W	MtF	07716	CEC	R94-1M	20
R224	10 MΩ	1%, 1 W	DCb	91637	DC-1	R13-10M	20
R225	10^8 Ω	1%, 2 W	DCb	91637	DC-2	R14-10^8	20

RESISTORS (cont'd)

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
R226	10^9 Ω	-	GCb	63060	RX-1	R20-10^9	20
R227	10^{10} Ω	-	GCb	63060	RX-1	R20-10^{10}	20
R228	15 Ω	10%, 1/4 W	Comp	44655	RC07	R76-15	18
R229	10 kΩ	10%, 1/4 W	Comp	44655	RC07	R76-10k	18
R230	220 kΩ	10%, 1/4 W	Comp	44655	RC07	R76-220k	18
R231	330 kΩ	10%, 1/4 W	Comp	44655	RC07	R76-330k	18
R232	100 kΩ	1/2 W	CbVar	80294	3068P	RP-63-100k	18
R233	1 MΩ	1/2 W	CbVar	80294	3068P	RP-63-1M	18
R234	1 MΩ	1/2 W	CbVar	80294	3068P	RP-63-1M	18

TRANSISTORS

Circuit Desig.	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
Q201	Dual, FET	32293	2N5452	TG-70	18
Q202	Silicon	04713	2N5089	TG-62	18
Q203	-	04713	2N3903	TG-49	18
Q204	-	04713	2N3905	TG-53	18

MOTHER BOARD PARTS LIST
("300" SERIES, PC-290)

CAPACITORS

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
C301	200 μF	35 V	EAL	90201	MTV	C177-200M	17
C302	200 μF	35 V	EAL	90201	MTV	C177-200M	17
C303	10 μF	20 V	ETT	17554	TSD1-20	C179-10M	17
C304	10 μF	20 V	ETT	17554	TSD1-20	C179-10M	17
C305	220 pF	1000 V	CerD	72982	-	C64-220P	17
C306	200 μF	35 V	EAL	90201	MTV	C177-200M	17
C307	200 μF	35 V	EAL	90201	MTV	C177-200M	17
C308	10 μF	20 V	ETT	17554	TSD1-20	C179-10M	17
C309	220 pF	1000 V	CerD	72982	-	C64-220P	17
C310	10 μF	20 V	ETT	17554	TSD1-20	C179-10M	17
C311	200 μF	35 V	EAL	90201	MTV	C177-200M	17
C312	10 μF	20 V	ETT	17554	TSD1-20	C179-10M	17
C313	.47 μF	20 V	ETT	17554	TSD1-20	C179-.47M	17
C314	10 μF	20 V	ETT	17554	TSD1-20	C179-10M	17

DIODES

Circuit Desig.	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
D301	Four Diode Bridge	83701	PD-10	RF-36	17
D302	Four Diode Bridge	83701	PD-10	RF-36	17
D303	Silicon	01295	1N645	RF-14	17
D304	Silicon	01295	1N645	RF-14	17
D305	Silicon	01295	1N914	RF-28	17
D306	Silicon	01295	1N914	RF-28	17
D307	Silicon	01295	1N914	RF-28	17

DIODES (cont'd)

Circuit Desig.	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
D308	Silicon	01295	1N914	RF-28	17
D309	Silicon	01295	1N914	RF-28	17
D310	Silicon	01295	1N914	RF-28	17

MISCELLANEOUS

Circuit Desig.	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
J301	Connector, Mini-PV	22526	47439	CS-236	17
J302	Connector, Mini-PV	22526	47439	CS-236	17
QA301	Integrated Circuit, Voltage Regulator	07263	UGA7723393	IC-25	17
QA302	Integrated Circuit, Voltage Regulator	07263	UGA7723393	IC-25	17
QA303	Integrated Circuit	07263	A749C	IC-27	17
S301	Switch, Line Voltage		-	SW-318	3
S302	Switch, "PUSH ON"		-	SW-340	3
S303	Switch, CURRENT SUPPRESS		-	SW-339	20
Q301	Transistor	02735	40312	TG-54	17
Q302	Transistor	02735	40312	TG-54	17
Q303	Transistor	07263	2N3565	TG-39	17
S304	Switch, POLARITY		-	SW-236	3
F301	Fuse, 117V, .25A, Slo-Blo, 3 AG	75915	313.250	FU-17	3
F301	Fuse, 234V, 1/8A, Slo-Blo, 3 AG	71400	MDL	FU-20	3
T301	Transformer	80164	-	TR-138	20
P305	Receptacle, AC	82389	AC3G	CS-235	3

RESISTORS (* Located on Switch S303.)

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
R301	634 Ω	1%, 1/8 W	MtF	07716	CEA	R88-634	17
R302	8.2 Ω	5%, 1/2 W	Comp	01121	EB	R19-8.2	17
R303	1.37 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1.37k	17
R304	200 Ω	0.5 W	-	80294	3329P	RP-88-200	17
R305	1.1 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1.1k	17
R306	634 Ω	1%, 1/8 W	MtF	07716	CEA	R88-634	17
R307	8.2 Ω	5%, 1/2 W	Comp	01121	EB	R19-8.2	17
R308	1.37 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1.371	17
R309	200 Ω	0.5 W	-	80294	3329P	RP-98-200	17
R310	1.1 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1.1k	17
R311	9.09 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-9.09k	17
R312	14 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-14k	17
R313	1 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1k	17
R314	10 Ω	10%, 1/4 W	Comp	44655	RC07	R76-10	17
R315	1 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1k	17
R316	9.09 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-9.09k	17
R317	1 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1k	17
R318	1 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-1k	17
R319	14 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-14k	17
R320	10 Ω	10%, 1/4 W	Comp	44655	RC07	R76-10	17
R321	10 kΩ	10%, 1/4 W	Comp	44655	RC07	R76-10k	17
R322	10 kΩ	10%, 1/4 W	Comp	44655	RC07	R76-10k	17
R323	330 Ω	10%, 1/4 W	Comp	44655	RC07	R76-330	17
R324	47 kΩ	10%, 1/4 W	Comp	44655	RC07	R76-47k	17
*R325	10 kΩ	1%, 1/2 W	MtF	07716	CEC	R94-10k	20

RESISTORS (cont'd)

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.	Fig. Ref.
* R326	100 kΩ	1%, 1/2 W	MtF	07716	CEC	R94-100k	20
* R327	1 MΩ	1%, 1/2 W	MtF	07716	CEC	R94-1M	20
* R328	10 MΩ	1%, 1 W	DCb	91637	DC-1	R13-10M	20
* R329	100 MΩ	1%, 2 W	DCb	91637	DC-2	R14-100M	20
* R330	10^9 Ω	-	GCb	63060	RX-1	R20-10^9	20
* R331	10^{10} Ω	-	GCb	63060	RX-1	R20-10^{10}	20
* R332	10^{11} Ω	-	GCb	63060	RX-1	R20-10^{11}	20
R333	10 kΩ	2 W	WW	12697	62JA	RP-92-10k	17
R334	100 kΩ	10%, 1/2 W	Comp	01121	EB	R1-100k	17

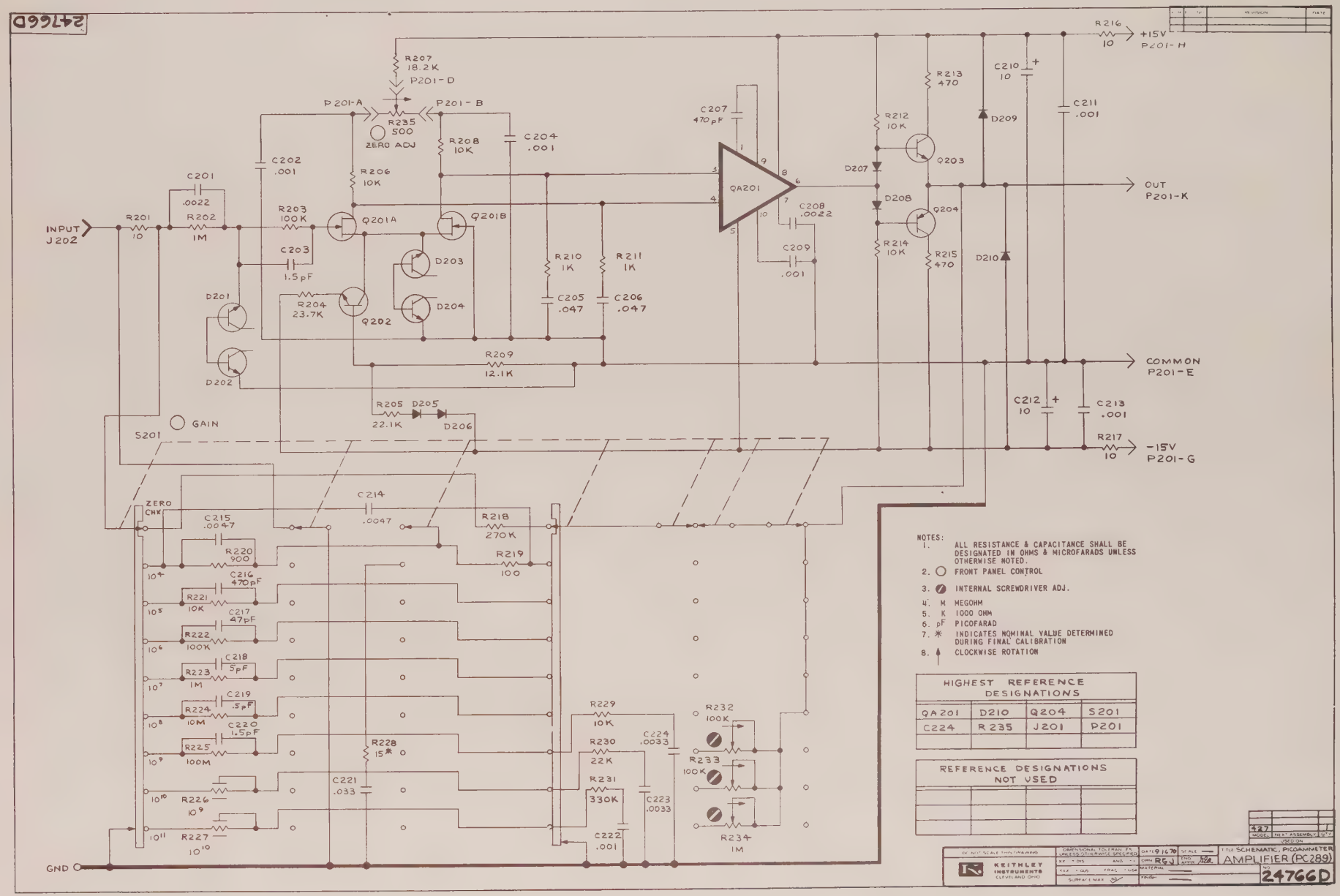
CODE TO NAME List (Continued).

63060	Victoreen Instrument Co. 5806 Hough Ave. Cleveland, Ohio 44103
70309	Allied Control Co., Inc. 2 East End Ave. New York, N.Y.
70903	Belden Mfg. Co. 415 So. Kilpatrick Chicago, Ill. 60644
71002	Birnbach Radio Co., Inc. 147 Hudson St. New York, N.Y.
71279	Cambridge Thermionic Corp. 430 Concord Avenue Cambridge, Mass.
71400	Bussmann Mfg. Div. of McGraw-Edison Co. St. Louis, Mo.
71450	CTS Corp. 1142 W. Beardsley Ave. Elkhart, Ind.
71468	ITT Cannon Electric, Inc. 3208 Humbolt St. Los Angeles, Calif. 90031
71590	Centralab Div. of Globe-Union, Inc. Milwaukee, Wisc. 53212
71785	Cinch Mfg. Co. and Howard B. Jones Div. Chicago, Ill. 60624
72619	Dialight Corp. 60 Stewart Ave. Brooklyn, N.Y. 11237
72653	G-C Electronics Co. 400 S. Wyman Rockford, Ill. 61101
72699	General Instrument Corp. Capacitor Division Newark, N.J. 07104
72982	Erie Technological Prods Inc. 644 W. 12th St. Erie, Pa. 16512
73138	Beckman Instruments, Inc. Helipot Division Fullerton, Calif. 92634
73445	Amperex Electronic Co., Div. of North American Philips Co., Inc. Hicksville, N.Y.
73690	Elco Resistor Co. 1158 Broadway New York, N.Y.
74276	Signalite Inc. 1933 Heck Ave. Neptune, N.J. 07753
74970	Johnson, E. F., Co. 297 Tenth Ave. S.W. Waseca, Minn. 56093
75042	IRC Inc. 401 North Broad St. Philadelphia, Pa. 19108
75915	Littlefuse, Inc. 800 E. Northwest Hwy. Des Plaines, Ill. 60016
76055	Mallory Controls, Div. of Mallory P. R. & Co., Inc. Frankfort, Ind.
76493	Miller, J. W. Co. 5915 S. Main St. Los Angeles, Calif. 90003
76545	Mueller Electric Co. 1583 E. 31st St. Cleveland, Ohio 44114
77764	Resistance Products Co. 914 S. 13th St. Harrisburgh, Pa. 17104
79727	Continental-Wirt Electronics Corp. Philadelphia, Pa.
80164	Keithley Instruments, Inc. 28775 Aurora Road Cleveland, Ohio 44139
80294	Bourns, Inc. 6135 Magnolia Ave. Riverside, Calif. 92506
81073	Grayhill, Inc. 561 Hillgrove Ave. La Grange, Ill. 60525
81483	International Rectifier Corp. 1523 East Grand Ave. El Segundo, Calif.
82389	Switchcraft, Inc. 5527 N. Elston Ave. Chicago, Ill. 60630
83125	General Instrument Corp. Capacitor Division Darlington, S.C. 29532
83330	Smith, Herman H., Inc. 812 Snediker Ave. Brooklyn, N.Y. 11207
83594	Burroughs Corp. Electronic Components Div. Plainfield, N.J. 07061
83701	Electronic Devices, Inc. Brooklyn, New York
84171	Arco Electronics, Inc. Community Drive Great Neck, N.Y. 11022
84411	TRW Capacitor Div. 112 W. First St. Ogallala, Nebr.
84970	Sarkes Tarzian, Inc. E. Hillside Dr. Bloomington, Ind.
86684	Radio Corp. of America Electronic Components & Devices Harrison, N.J.
87216	Philco Corp. Lansdale Div., Church Rd. Lansdale, Pa. 19446
90201	Mallory Capacitor 3029 East Washington Indianapolis, Ind. 46206
90303	Mallory Battery Co. Tarrytown, New York
91637	Dale Electronics, Inc. P.O. Box 609 Columbus, Nebr. 68601
91662	Elco Corp. Willow Grove, Pennsylvania
91737	Gremar Mfg. Co., Inc. 7 North Ave. Wakefield, Mass.
91802	Industrial Devices Inc. 982 River Rd. Edgewater, N.J. 07020
91929	Honeywell Inc. Micro Switch Div. Freeport, Ill. 61032
93332	Sylvania Electric Products, Inc. Semiconductor Products Div. Woburn, Mass.
93656	Electric Cord Co. 1275 Bloomfield Ave. Caldwell, N.J.
94144	Raytheon Co., Industrial Operation Components Div. Quincy, Mass.
94154	Tung-Sol Electric, Inc. Newark, New Jersey
94310	Tru-Ohm Products Memcor Components Div. Huntington, Ind. 46750
94696	Magnecraft Electric Co. 5579 North Lynch Chicago, Ill.
95348	Gordos Corp. 250 Glenwood Ave. Bloomfield, N.J. 07003
95712	Dage Electric Co., Inc. Hurricane Road Franklin, Ind.
97933	Raytheon Co. Components Div. Semiconductor Operation Mountain View, Calif.
99120	Plastic Capacitors, Inc. 2620 N. Clybourn Ave. Chicago, Ill.

CODE—TO—NAME LIST

CODE TO NAME List of Suggested Manufacturers.
Reference: Federal Supply Code for Manufacturers, Cataloging Handbook H4-2.

00656	Aerovox Corp. 740 Belleville Ave. New Bedford, Mass. 02741
00686	Film Capacitors, Inc. 100 Eighth St. Passaic, N.J.
01121	Allen-Bradley Corp. 1201 South 2nd St. Milwaukee, Wisc. 53204
01295	Texas Instruments, Inc. Semiconductor-Components Div. Dallas, Texas 75231
01686	RCL Electronics, Inc. 195 McGregor St. Manchester, N.H. 03102
02101	Varo Inc. Electrokinetics Div. Santa Barbara, Calif. 93102
02660	Amphenol Corp. 2801 South 25th Ave. Broadview, Ill. 60153
02734	Radio Corp. of America Defense Electronic Products Camden, N.J.
02735	Radio Corp. of America Receiving Tube Div. Somerville, N.J.
02777	Hopkins Engineering Co. 12900 Foothill Blvd. San Fernando, Calif. 91342
02985	Tepro Electric Corp. 5 St. Paul St. Rochester, N.Y. 14604
03508	General Electric Co. Semiconductor Products Dept. Syracuse, N.Y. 13201
04009	Arrow-Hart & Hegeman Electric Co. 103 Hawthorne St. Hartford, Conn. 06106
04713	Motorola Semiconductor Prod. Inc. 5005 E. McDowell Rd. Phoenix, Ariz. 85008
05079	Tansistor Electronics, Inc. 1000 West Road Bennington, Vt. 05201
05397	Union Carbide Corp. Electronics Div. New York, N.Y. 10017
06751	Components, Inc. Arizona Div. Phoenix, Ariz. 85019
06980	Varian Assoc. EIMAC Div. 301 Industrial Way San Carlos, Calif. 94070
07137	Transistor Electronics Corp. Hwy. 169 - Co. Rd. 18 Minneapolis, Minn. 55424
07263	Fairchild Camera & Inst. Corp. 313 Frontage Road Mountain View, Calif.
07716	IRC, Inc. 2850 Mt. Pleasant Burlington, Iowa 52601
08811	GL Electronics Div. of GL Industries, Inc. Westville, N.J. 08093
09052	Gulton Industries, Inc. Alkaline Battery Div. Metuchen, N.J.
09823	Burgess Battery Co. Div. of Servel Inc. Freeport, Ill.
09922	Burndy Corp. Richards Ave. Norwalk, Conn. 06852
10582	CTS of Asheville Inc. Mills Gap Road Skyland, N.C.
11502	IRC Inc. Greenway Road Boone, N.C. 28607
11837	Electro Scientific Indus., Inc. 13645 NW Science Park Dr. Portland, Or. 97229
12040	National Semiconductor Corp. Commerce Drive Danbury, Conn. 06813
12065	Transitron Electronic Corp. 144 Addison St. East Boston, Mass.
12697	Clarostat Mfg. Co., Inc. Lower Washington St. Dover, N.H. 03820
12954	Dickson Electronics Corp. 302 S. Wells Fargo Ave. Scottsdale, Ariz.
13050	Potter Co. Highway 51 N. Wesson, Miss. 39191
13327	Solitron Devices, Inc. 256 Oak Tree Road Tappan, N.Y. 10983
13934	Midwec Corp. 602 Main Oshkosh, Nebr. 69154
14655	Cornell-Dubilier Electric Corp. 50 Paris Street Newark, N.J.
14659	Sprague Electric Co. P.O. Box 1509 Visalia, Calif. 93278
15238	ITT Semiconductors Div. of ITT Corp. Lawrence, Mass. 01841
15909	Daven Div. of T.A. Edison Ind. McGraw Edison Co. Livingston, N.J.
16170	Teledyne Systems Co. Communications Div. Los Angeles, Calif. 90066
17554	Components, Inc. Smith St. Biddeford, Ma. 04005
23020	General Reed Co. 174 Main St. Metuchen, N.J. 08840
24655	General Radio Co. 22 Baker Ave. West Concord, Mass. 01781
27682	Hathaway Instruments, Inc. 5800 E. Jewell Ave. Denver, Colorado 80222
28520	Heyman Mfg. Co. 147 N. Michigan Ave. Kenilworth, N.J.
29309	Richey Electronics Inc. 1307 Dickerson Rd. Nashville, Tenn. 37213
35529	Leeds and Northrup 4901 Stenton Ave. Philadelphia, Pa. 19144
37942	Mallory, P. R. and Co., Inc. 3029 E. Washington St. Indianapolis, Ind. 46206
44655	Ohmite Mfg. Co. 3601 Howard St. Skokie, Ill. 60076
53201	Sangamo Electric Co. 1301 North 11th Springfield, Ill. 62705
54294	Shallcross Mfg. Co. 24 Preston St. Selma, N.C.
56289	Sprague Electric Co. North Adams, Massachusetts
58474	Superior Electric Co., The 383 Middle St. Bristol, Conn. 06012
61637	Union Carbide Corp. 270 Park Ave. New York, N.Y. 10017



NOTES:
1. ALL RESISTANCE & CAPACITANCE SHALL BE DESIGNATED IN OHMS & MICROFARADS UNLESS OTHERWISE NOTED.
2. ○ FRONT PANEL CONTROL
3. ⊘ INTERNAL SCREWDRIVER ADJ.
4. M MEGOHM
5. K 1000 OHM
6. pF PICOFARAD
7. * INDICATES NOMINAL VALUE DETERMINED DURING FINAL CALIBRATION
8. ↑ CLOCKWISE ROTATION

HIGHEST REFERENCE DESIGNATIONS			
QA201	D210	Q204	S201
C224	R235	J201	P201

REFERENCE DESIGNATIONS NOT USED			

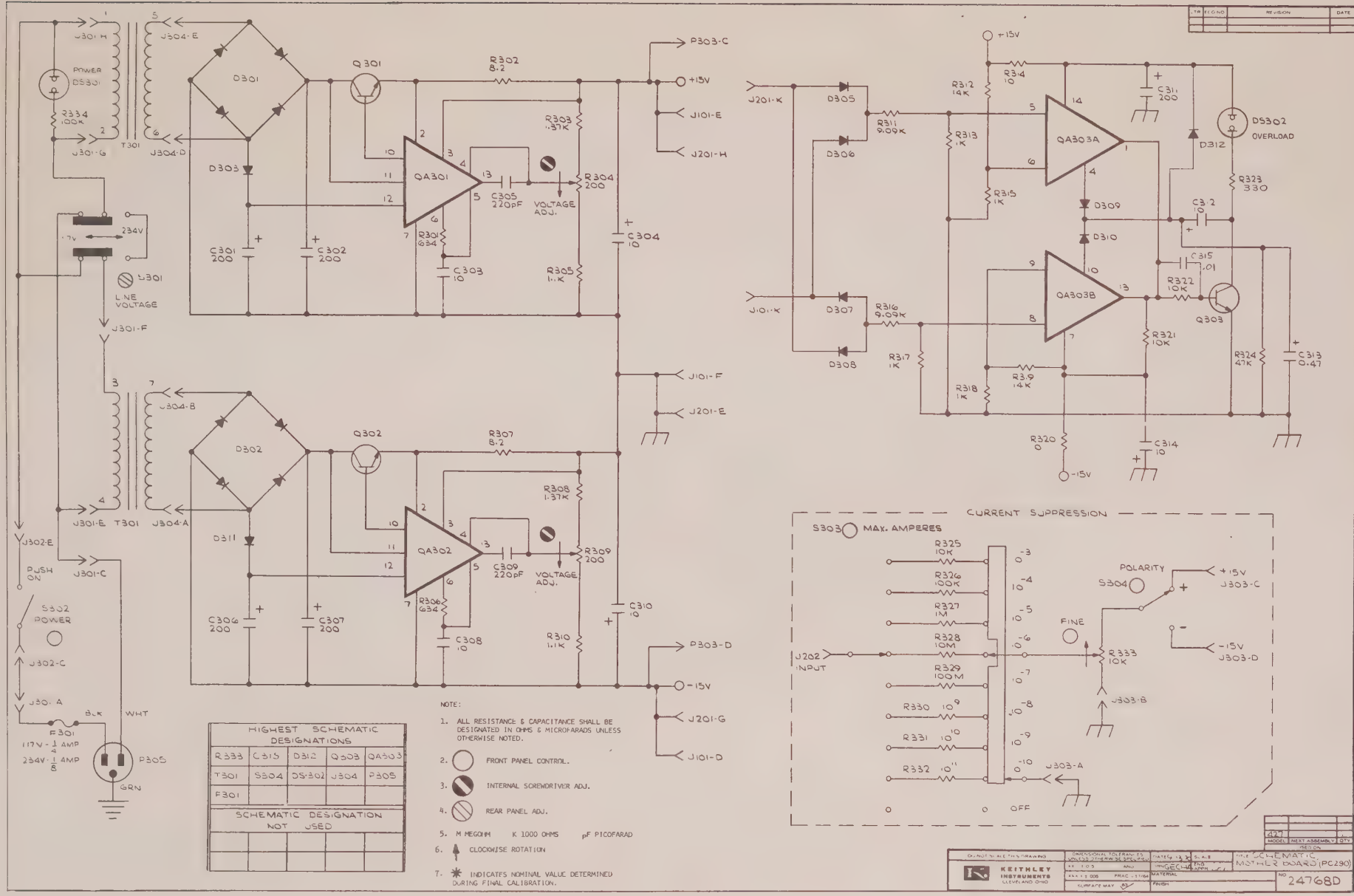
KEITHLEY INSTRUMENTS CLEVELAND OHIO

DRAWN RSJ 9/6/78 SCALE —

TITLE SCHEMATIC, PICOAMMETER AMPLIFIER (PC289)

NO. 24766D

427



HIGHEST SCHEMATIC DESIGNATIONS				
R333	C315	D312	Q303	QA303
T301	S304	DS302	J304	P305
F301				

SCHEMATIC DESIGNATION NOT USED				

NOTE:

1. ALL RESISTANCE & CAPACITANCE SHALL BE DESIGNATED IN OHMS & MICROFARADS UNLESS OTHERWISE NOTED.
2. ○ FRONT PANEL CONTROL.
3. ⊘ INTERNAL SCREWDRIVER ADJ.
4. ⊘ REAR PANEL ADJ.
5. M MEGOHM K 1000 OHMS pF PICOFARAD
6. CLOCKWISE ROTATION
7. ✳ INDICATES NOMINAL VALUE DETERMINED DURING FINAL CALIBRATION.

TR	ECO NO.	REVISION	DATE

DO NOT SCALE THIS DRAWING	DIMENSIONAL TOLERANCE UNLESS OTHERWISE SPECIFIED	DATE	SCALE
KEITHLEY INSTRUMENTS CLEVELAND OHIO	XX ± .03 ANG	DRAWN GECH	FILE
	XXX ± .005 FRAC ± 1/64	MATERIAL	
	SURFACE MAY ✓	FINISH	

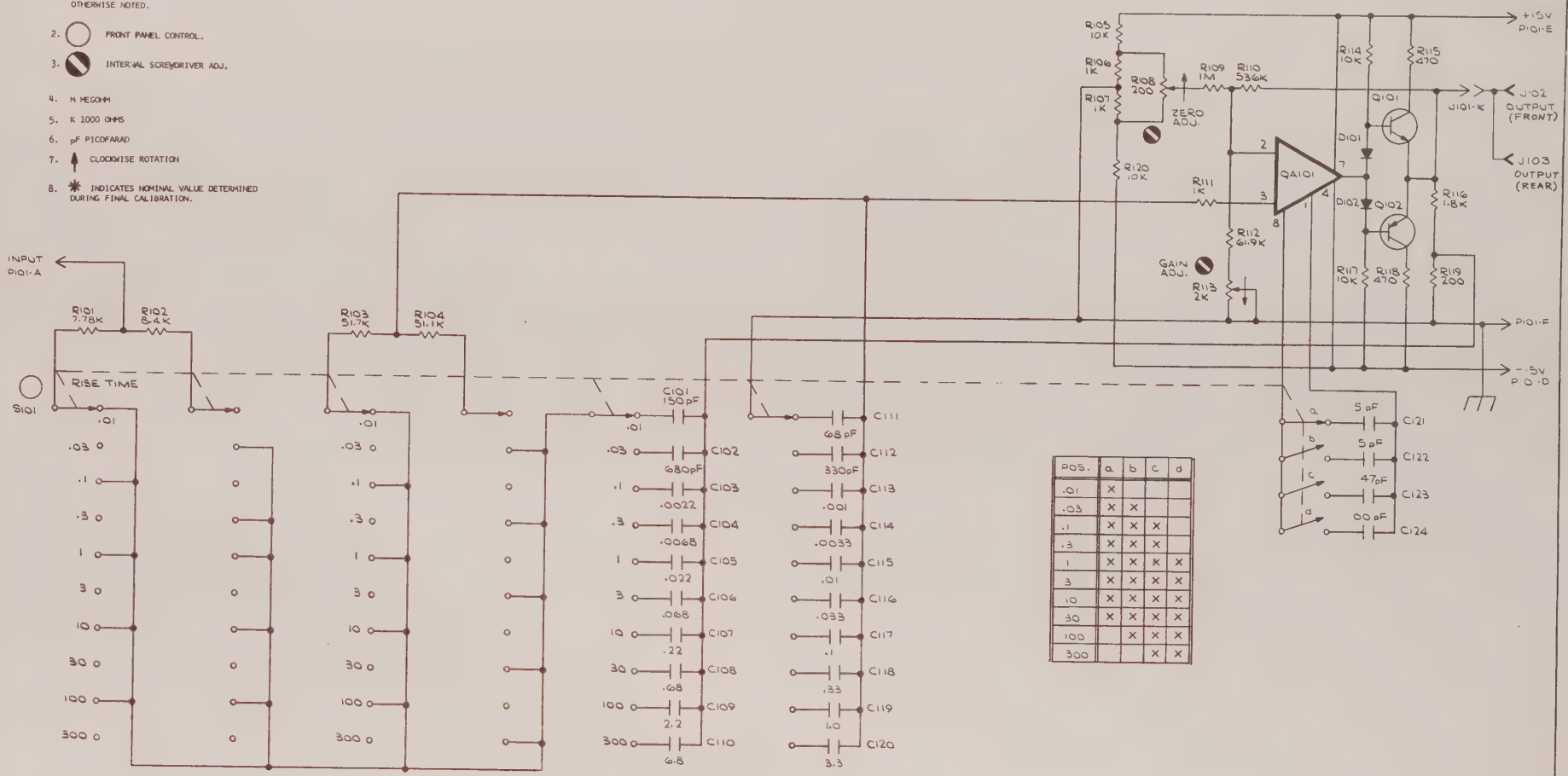
MODEL	NEXT ASSEMBLY	QTY
	USED ON	

TITLE SCHEMATIC, MOTHER BOARD (PC290)

NO 24768D

NOTE:

1. ALL RESISTANCE & CAPACITANCE SHALL BE DESIGNATED IN OHMS & MICROFARADS UNLESS OTHERWISE NOTED.
2. ◯ FRONT PANEL CONTROL.
3. ⊘ INTERNAL SCREWDRIVER ADJ.
4. M MEGOHM
5. K 1000 OHMS
6. pF PICOFARAD
7. ↻ CLOCKWISE ROTATION
8. ✱ INDICATES NOMINAL VALUE DETERMINED DURING FINAL CALIBRATION.



POS.	a	b	c	d
.01	X			
.03	X	X		
.1	X	X	X	
.3	X	X	X	
1	X	X	X	X
3	X	X	X	X
10	X	X	X	X
30	X	X	X	X
100		X	X	X
300			X	X

HIGHEST SCHEMATIC DESIGNATIONS				
R120	C124	D102	Q102	QA101
S101	P101	J102		

SCHEMATIC DESIGNATIONS NOT USED				

REVISION	DATE

MODEL	NEXT ASSEMBLY	QTY
237		

USED ON

DO NOT SCALE THIS DRAWING

KEITHLEY INSTRUMENTS CLEVELAND OHIO

DIMENSIONAL TOLERANCES UNLESS OTHERWISE SPECIFIED: XX ± .010 AND ± 1°, XXX ± .005 FRAC ± 1/64, SURFACE MAX 63

DATE 7-13-76 DRNG CHA APPR

SCALE TWO

MATERIAL

FINISH

TITLE SCHEMATIC FILTER BOARD (PC292)

NO 247670

REPAIR AND CALIBRATION FORM

For repair or calibration, please fill out this form and return it with your instrument to:

Sales Service Department
Keithley Instruments, Inc.
28775 Aurora Road
Cleveland, Ohio 44139

R-_____
Do not write in this space.

User's Name _____ Telephone _____ Ext. _____
Company _____ Address _____
Division _____ City _____ State _____ Zip _____
Date _____ Model No. _____ Serial No. _____

1. Reason for Return
   - ☐ Repair and Recalibration
   - ☐ Recalibration only (No report, except as specified in item 4 on reverse)*

   *If repairs are necessary to meet specifications, they will be in addition to the calibration.

2. Calibration Report Desired
   - ☐ Report of Calibration Certified Traceable to N.B.S.
   - ☐ Calibration Report
   - ☐ Certificate of Compliance
   - ☐ None

   (for details, see reverse side of this form)

3. To help repair the instrument, briefly describe the problem: _____

4. Is the problem ☐ Constant ☐ Intermittant
   Under what conditions does the problem occur:
   a) Control setting _____
   b) Approx. Temperature _____ °F
   c) Approx. Temperature variation ± _____ °F
   d) Approx. Humidity (high, medium, low) _____
   e) Line voltage _____
   f) Other (such as line transients, line variations, etc.) _____

5. Please draw a block diagram of the system using the Keithley. List any other pertinent data which can help in the repair. Include charts or other data if available.
   Signal Source _____
   Source Impedance _____
   Readout Device:
   - ☐ Recorder
   - ☐ Oscilloscope
   - ☐ Other
   - ☐ None

   Lengths & Types of Connecting Cables _____

6. What repairs or modifications have been made on this instrument which are not on file with the Keithley Repair Department? _____

7. Please enclose any other pertinent data and charts which you feel might help the Repair and Calibration Department

_____ Signature _____ Title

CALIBRATIONS AVAILABLE AT KEITHLEY INSTRUMENTS.

Listed and defined below are the four types of calibrations and their associated report formats which are presently available at Keithley Instruments. They fall into the following categories:

1. Report of Calibration Certified Traceable to the National Bureau of Standards
2. Calibration Report
3. Certificate of Compliance
4. Recalibration

All calibration and certification performed by Keithley Instruments is in accord with MIL-C-45662A.

Prices shown below are in addition to repair charges for any work necessary to place a customer's unit into first class condition prior to the calibration.

I. Report of Calibration Certified Traceable to the National Bureau of Standards.

This is a completely documented report, including all basic errors or deviations from nominal settings on appropriate ranges, terminals, dials, etc. Work is performed using the primary standards of the company with secondary transfers kept to a minimum. The NBS test numbers for the latest recalibration of the primary standards are furnished.

By definition, the above is performed in our Standards Laboratory so that random operator induced error is minimized and maximum protection to the equipment used is maintained.

This type of calibration is not recommended for instruments with a basic inaccuracy of 1% or greater. The precision involved in this report makes it uneconomical for such instruments. The Calibration Report listed below (No. 2) would be better suited in this case.

As of 11/1/69 the Report of Calibration Certified Traceable to the National Bureau of Standards is available on the following instruments at the prices listed:

Model 140	$275	Model 5155 (Complete Set)	$295
Model 260	$225	Model 5155-10^{8}	$ 50
Model 261	$375	Model 5155-10^{9}	$ 50
Model 515	$375	Model 5155-10^{10}	$ 50
Model 630	$275	Model 5155-10^{11}	$ 60
Model 660A	$250	Model 5155-10^{12}	$ 60
Model 662	$275	Model 5155-10^{13}	$ 80

2. Calibration Report.

This report shows only the cardinal range, terminal, dial, etc. errors as determined by production calibration equipment and personnel. The production equipment is maintained traceable by transfer techniques against the primary standards maintained by the company. We attest to this fact and list basic deviations from nominal but the conditions of calibration are not as precisely controlled as the previous report nor are NBS test numbers supplied.

This report is available for any instrument in our line. As of November 1, 1969, only the following price has been established for this report:

Model 261 . . . . . $ 55

Prices for other units can be estimated upon request.

3. Certificate of Compliance.

This is merely a restatement of the basic guarantee that the instrument was calibrated on equipment that is maintained by our standards personnel against primary standards. No report is issued.

This Certificate of Compliance is available at no charge for any instrument with the exception of the Model 261.

A newly purchased Model 261 or one returned for repair or recalibration is automatically supplied with a Calibration Report (as described in (2) above). The nature of this instrument makes it necessary to complete this report to ascertain specified accuracy. This Calibration Report is forwarded to the customer with the instrument. The $55 charge is incorporated as part of the normal calibration charge of the Model 261.

4. Recalibration.

This is a recalibration of the instrument according to our factory calibration procedures. The prices for this as of November 1, 1969 are as follows:

Model 260 . . . . . $ 85 (No report supplied. A Certificate of Compliance can be had at no charge if requested).

Model 261 . . . . . $ 55 (Calibration Report as described in (2) above is supplied. See (3) for explanation).

All other instruments are on a time and material basis for the particular unit involved.

CHANGE NOTICE

July 21, 1972 MODEL 427 CURRENT AMPLIFIER

Page 20. Change to the following:

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.
R105	10 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-10K

Add the following:

Circuit Desig.	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.
-	Cap, BNC, mates with J102	02660	31-007	CAP-18

Page 21. Change to the following:

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.
R120	10 kΩ	1%, 1/8 W	MtF	07716	CEA	R88-10K
C215	0.0047 µF	1000 V	CerD	56289	10SS-D47	C64-.0047M
C223	0.0033 µF	1000 V	CerD	56289	10SS-D33	C22-.0033M
C224	0.0033 µF	1000 V	CerD	56289	10SS-D33	C22-.0033M

Page 23. Change to the following:

Circuit Desig.	Value	Rating	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.
R228	*15 Ω	10%, 1/4 W	Comp	44655	RC07	R76-15
R232	100 kΩ	.75 W	Comp	80294	3009P	RP89-100K
R233	1 MΩ	.75 W	Comp	80294	3009P	RP89-1M
R234	1 MΩ	.75 W	Comp	80294	3009P	RP89-1M

*Nominal value, selected in test.

Circuit Desig.	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.
Q201	Dual, FET, TO-71 Case	80164	-	25099A*

*Selected TG-70

Page 24. Change to the following:

Circuit Desig.	Type	Mfr. Code	Mfr. Desig.	Keithley Part No.
Q303	Silicon, NPN, TO-92 Case	04713	2N3903	TG-49

REF: PCM 1348/0271

MP MASTER
MA35146

KEITHLEY INSTRUMENTS, INC.

28775 AURORA ROAD • CLEVELAND, OHIO 44139 • (216) 248-0400
TELEX: 98-5469 • CABLE: KEITHLEY